

140

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FIELD BOOK

740

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B. K. EBELT COMPANY

PLEASE RETURN TO  
GEAUGA COUNTY ENGINEER

TABLE FOR REDUCING PERCHES TO FEET AND INCHES.

PERCH	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.
1	16.6 in.	21	3.40 6 in.	41	6.76.6 in.	61	10.06.6 in.	81	13.36.6 in.		
2	33.0	22	3.63.0	42	6.93.0	62	10.23.0	82	13.53.0		
3	49.6	23	3.79.6	43	7.09.6	63	10.39.6	83	13.69.6		
4	66.0	24	3.96.0	44	7.26.0	64	10.56.0	84	13.86.0		
5	82.6	25	4.12.6	45	7.42.6	65	10.72.6	85	14.02.6		
6	99.0	26	4.29.0	46	7.59.0	66	10.89.0	86	14.18.0		
7	1.15.6	27	4.45.6	47	7.75.6	67	11.05.6	87	14.34.6		
8	1.32.0	28	4.62.0	48	7.92.0	68	11.22.0	88	14.51.0		
9	1.48.6	29	4.78.6	49	8.08.6	69	11.38.6	89	15.07.6		
10	1.65.0	30	4.95.0	50	8.25.0	70	11.55.0	90	15.24.0		
11	1.81.6	31	5.11.6	51	8.41.6	71	11.71.6	91	15.40.6		
12	1.98.0	32	5.28.0	52	8.58.0	72	11.88.0	92	15.57.0		
13	2.14.6	33	5.44.6	53	8.74.6	73	12.04.6	93	16.13.6		
14	2.31.0	34	5.61.0	54	8.91.0	74	12.21.0	94	16.30.0		
15	2.47.6	35	5.77.6	55	9.07.6	75	12.37.6	95	16.46.6		
16	2.64.0	36	5.94.0	56	9.24.0	76	12.54.0	96	16.63.0		
17	2.80.6	37	6.10.6	57	9.40.6	77	12.70.6	97	16.79.6		
18	2.97.0	38	6.27.0	58	9.57.0	78	12.87.0	98	16.96.0		
19	3.13.6	39	6.43.6	59	9.73.6	79	13.03.6	99	17.12.6		
20	3.30.0	40	6.60.0	60	9.90.0	80	13.20.0	100	17.29.0		

COURT HOUSE  
CHARDON, O.  
PHONE 250-X

B. K. ELLIOTT COMPANY, PITTSBURG, PA.  
DRAWING MATERIALS AND SURVEYING INSTRUMENTS

Boon 140

Downings Corners, N. Road  
CH #4, Sec. P = Munson Twp Sec A  
CH #4, Sec. Q = Chardon Twp Sec B  
Page 1 - 20

Auburn  
Munson Center South Road  
N. end Sec. M  
See below Page 40

John Shafford Survey Page 76

Court Case Notes Pg 26

Chardon - Auburn Rd.  
#4 Sec. L-M (1946) Pgs. 49-56

Aub. Rd CH 4 Sec P & Q <sup>S.R</sup> pro File  
pg 67

Aub. Rd new culv't S of #6  
1950 pg 35

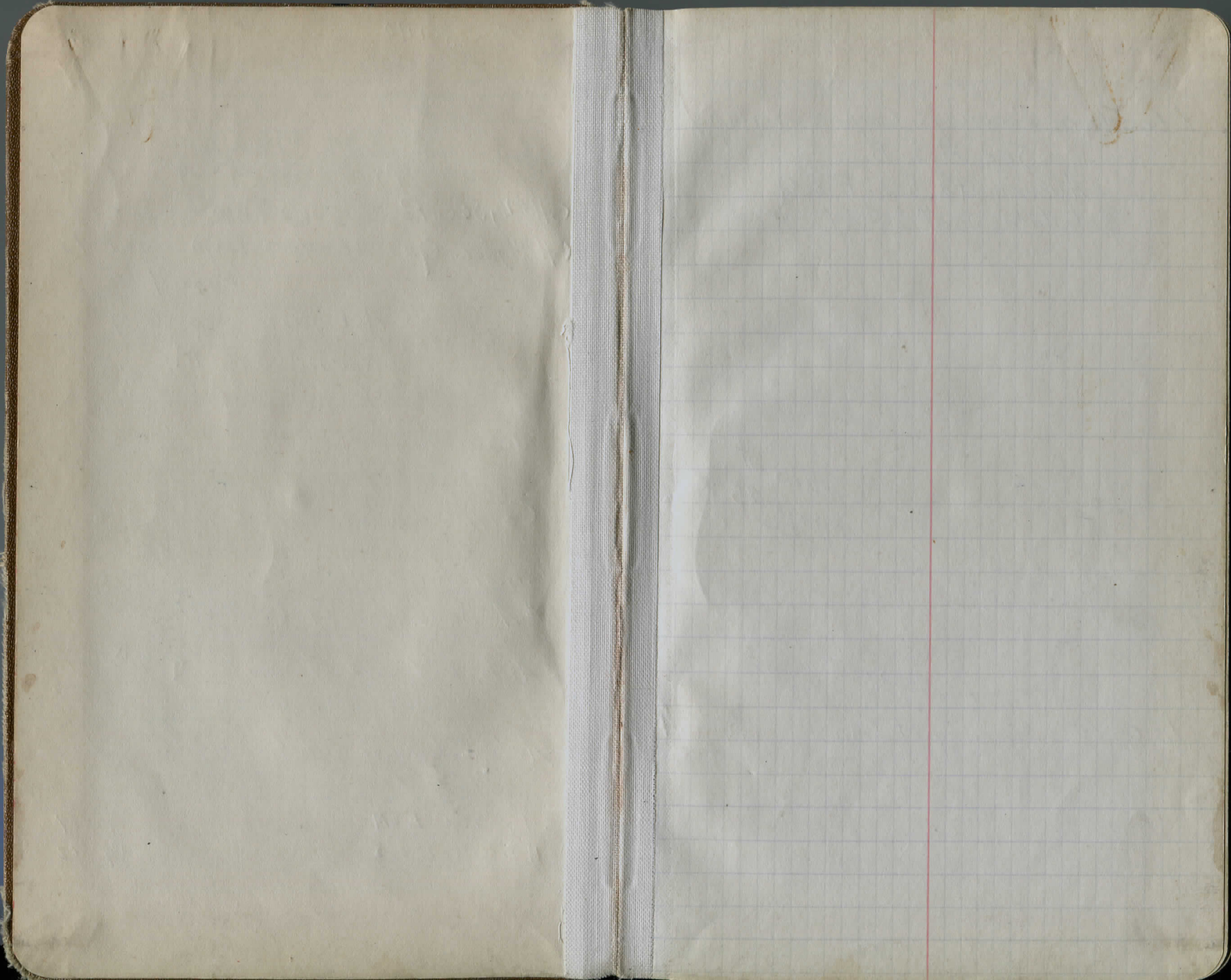
\* 4 X SEC L & M

Pg 57

\* 4 Profile SEC Q

Pg 72

140



Location Downings Corners North Rd  
 Sec A. & B.  
 = Auburn Rd Sec P & Q  
 sidestates set 25' Rt or East

Notes for detail of intersection at  
 Downings Cor. see page 25

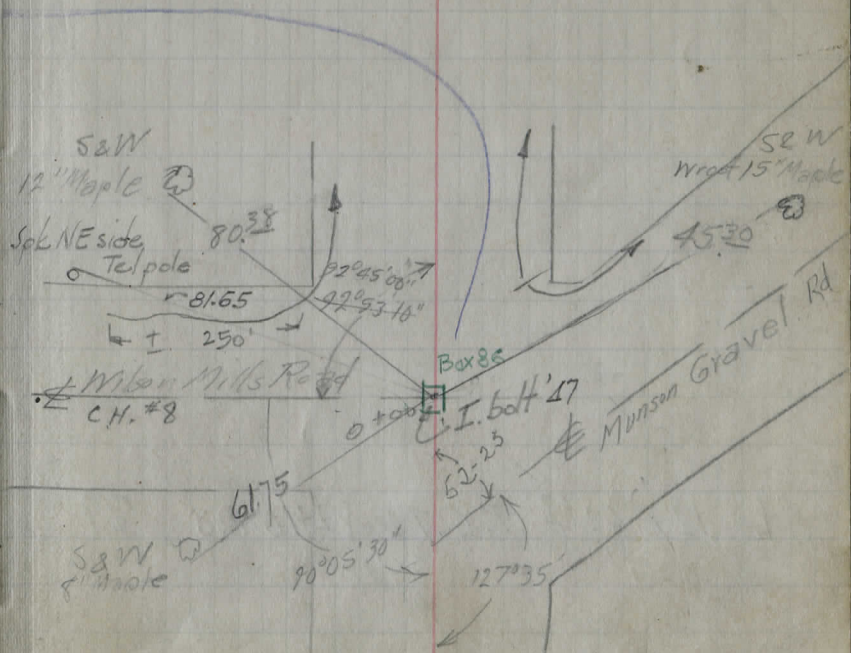
Sta 0+00 Beginning of Imp spike set

11/29/32  
 rest of 7/23/35

50-25  
 27-35  
 180-00  
 92-25  
 90-03-30  
 182-50-30  
 127-09-30

Build new 12" 36' long  
 8" Cor IP floor  
 Condition Flow Rt.  
 10' long

8+82 →



Sta 30+95<sup>00</sup> POT

Pin  
Set

Approx S Line Pfander



Box 87

2  
both Fd  
1/11/50

58W  
24" Maple

91.50

74.20

58W  
24" Maple

Extend 20' R Relay

12" CIP Culv.

good condition

Fl. Lt 13' long

28+76

Sta 20+10 Build new 12" Culvert

Sta 12+62<sup>18</sup> POT

Pin  
Set

pipe

Fd  
1/11/50

31.02



Box 87

pipe

Fd 1/1/50

180°

180°

Sta 43+58<sup>66</sup>

POT.

BOLTSET  
7-26-50Pin  
Set

10256

Remove  
8" Cor. IP Culv.  
poor condition ←53+253x3 Stone Box  
good condition ←

Fl. Lt. 18' long

49+49

9 93

Build new 4x3

SP. 11/4 SIDE  
C.E.I. 58A754June  
not found 87

112921

31<sup>88</sup>~~31<sup>85</sup>~~S&W  
SWroot  
15" MapleS&W 20" ASH  
SE. ROOT

10256

~~52<sup>16</sup>~~  
51<sup>95</sup>S&W  
Wroot  
30" MapleBuild new 18" 40' long  
Salvage old to 44+5612" CIP culvert  
good condition  
Fl. Lt. 16' long ←40+25

Extend 24' 2' Relay

18" VSP Culv.  
good condition ←34+00

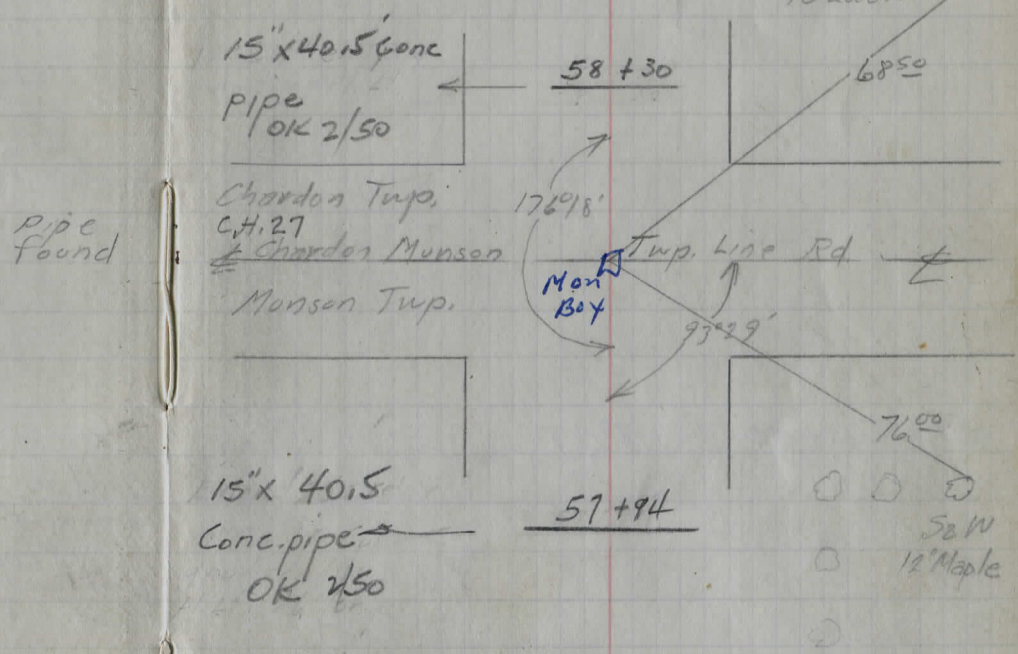
Fl. Lt. 16' long

1.10 miles Sec A.  
 5280 | 5811  
 3290  
 5310  
 5250

End of Sect. B  
 Sta 58+11.05 @ Twp. Line Rd.  
 End of Sect. A.

11.05  
 188.95

15" Cor IP & VSP  
 fair condition ← 64+17  
 Fl. Lt. 13 11



15" x 40.5' Conc  
 pipe  
 OK 2/50 ← 58+30

Chardon Twp.  
 Ch. 27  
 Chardon Munson  
 Munson Twp.  
 176.18'

15" x 40.5'  
 Conc. pipe ← 57+94  
 OK 2/50

Extend with sludge  
 from 40+25  
 12" CIP Con. ← 54+56  
 good condition  
 Fl. Lt. 14' long

Sta 76+50

POT

spike  
Set

3x2 Stone Box Culv.  
Conc. Slab  
fair condition

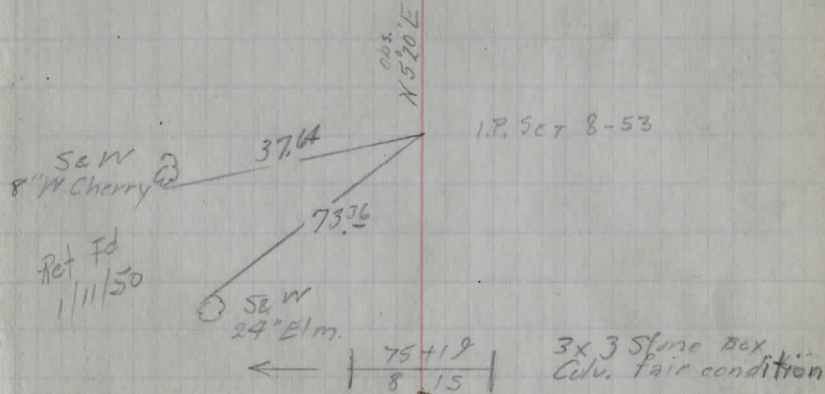
$$\left| \begin{array}{r} 89+23 \\ \hline 92 \quad 11 \end{array} \right|$$

15" Cor. IP Culv.  
good condition

$$\leftarrow \frac{87+13}{12 \quad 12}$$

6" CIP Culv.  
good condition

$$\leftarrow \frac{82+84}{10 \quad 15}$$



15" VSP Culv.  
fair condition  
Pl. Lt.

$$\leftarrow \frac{70+36}{12 \quad 14}$$

183 miles total

$$\begin{array}{r} 528 \overline{) 966039} \\ \underline{528} \\ 4380 \\ \underline{4224} \\ 1560 \end{array}$$

966039  
581165  
3849.33 = .73 miles Sec B

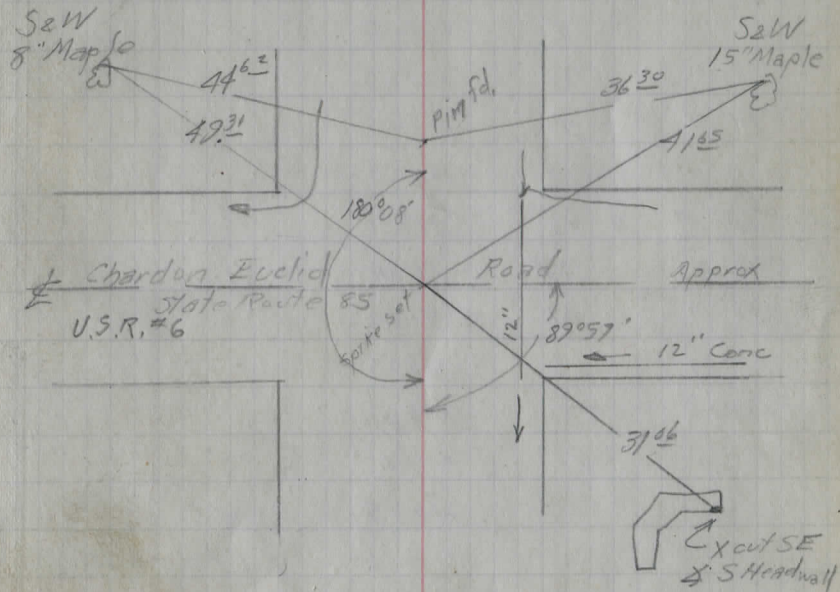
$$\begin{array}{r} 528 \overline{) 3849.33} \\ \underline{3696} \\ 1533 \end{array}$$

796

Sta 96+68.39

Sta 96+60.38 ± Chardon Euclid Rd Spike set

Pin found

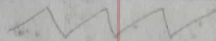


9668.34  
131.66 ✓  
9800.00

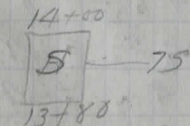
# Topography

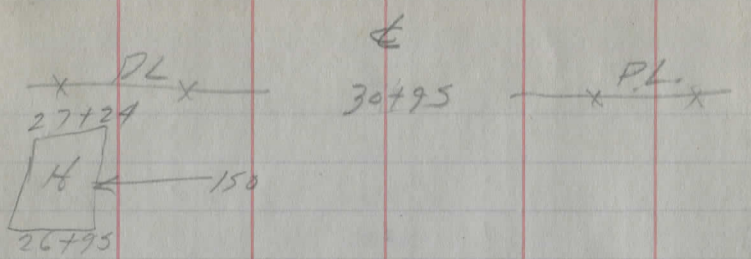


		13+00	25	2-6"Lo
		12+75	23	6"E
		12+65	22	2-10"Lo
		12+62		<del>PL</del>
<del>x</del>	<del>PL</del>			
14E	18	11+85		
10"M	21	11+80		
8"E	18	11+75		
12"M	24	11+50		
10"M	19	11+05		
10"M	20	10+85		
18"M	26	10+45		
18"M	18	10+25		
24"M	18	9+90		
10"M	19	9+50		
12"M	22	9+20		
10"M	23	8+95		
12"M	23	8+80		
10"Ap	19	4+70		
		4+35		
		2+90	17	18"NC
		1+20	14	18"Pe
15"M	23	0+75		
TCEI	24	0+50		



		17+50	24	6-4"Lo
		17+36	25	6"Lo
		17+10	24	2-6"Lo
		16+75	24	2-1"Lo
		16+66	24	2-8"NC
		16+30	25	8"M
		16+20	24	2-4"M
		15+85	24	2-8"M
		15+72	21	8"M
Drive		15+30		
		14+75		
		14+90		
		14+66	23	6"M
		14+63	23	6"M
		14+54	23	6"M
		14+36	23	4"M
		14+23	23	10"M
		14+15	23	4"Lo
		14+00		
		13+80		
		13+85	22	8"M
Drive		13+50		
		13+32	21	8"M

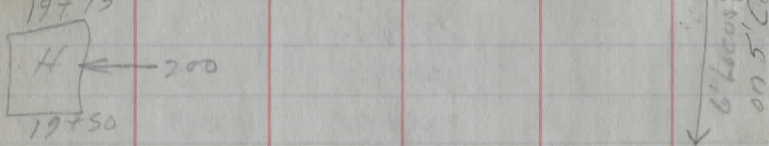




Drive 26+90  
26+85 ~~x~~ ~~x~~

4" A 20 25+90  
8" A 20 25+65  
4" O 20 23+70  
6" O 20 23+60  
6" WC 20 23+40

22+10 25 12" M  
8" A 18 21+75  
18" M 19 20+60  
Drive 19+60



18+75 24 2-10" Lo  
18+65 ~~x~~ ~~x~~  
18+60 24 2-8" Lo  
18+45 24 3-A" Lo  
18+25 24 3-A" E  
18+10 23 2-8" Lo  
17+85 23 8" Lo  
17+60 24 8" WC

6" West & Elm  
on 5' Center

35+15 19 4" M  
34+95 19 15" Stump  
34+90 21 4" M

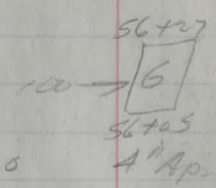
4" M 26 34+50  
15" M 26 34+40  
34+30 13 12" M  
12" M 22 34+25

33+90 14 24" E  
33+85 17 6" M  
33+75 18 6" M  
33+70 18 10" M  
33+65 21 6" M  
33+35 20 18" M  
33+25 18 12" M  
33+20 18 6" M

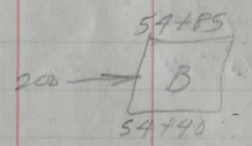
10" M 22 33+05  
32+95 20 10" M  
32+85 15 12" M

15" M 18 32+70  
4" M 18 32+20  
10" O 22 31+40  
8" M 14 31+25  
4" M 13 31+20  
10" WC 15 31+05  
6" M 22 30+95

⊕



55+98 20



53+95 10 48" Boulder

53+40 Drive

24" M 23 48+10

15" M 24 46+80

44+80 Drive

~~42+67~~

Drive 41+60

39+80 Drive

15" M 16 39+20

12" M 17 37+80

12" M 19 37+50

12" WC 21 37+20

4" M 20 37+10

4" M 21 37+00

36+80 19 10" M

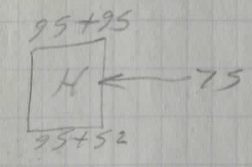
12" M 23 36+25

35+60 22 4" M

35+55 20 6" M

35+50 17 10" M

⊕



Drive 95+40

8" M 23 95+45

~~91+08~~

~~PL~~ 75+21

~~70+10~~

12" Ap 22 69+40

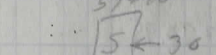
~~69+15~~

~~65+28~~

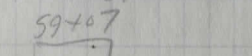
~~60+65~~ 2.5 12" Ap

~~59+75~~

Drive 59+50



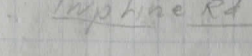
59+07



58+85

Tripline Rd 58+11

57+32



57+10 57+10

Drive

56+35



		1289.25		
10+0			5.2	84.1
11+0			7.2	82.1
12+0			8.4	80.9
13+0	397	1284.67	8.55	1280.70
			5.0	79.7
14+0			6.7	78.0
15+0			7.6	77.1
16+0			10.8	73.9
	0.34	1277.38	7.63	1277.04
17+0			6.8	70.6
18+0			7.8	69.6
19+0			8.0	69.4
	3.55	1273.60	7.33	1270.05
BM#3			5.81	1267.79
19+85 Prop. Culv.				1267.90
			4.8	68.8
20+0			5.2	68.4

$\frac{40}{25}$	$\frac{48}{24}$	$\frac{44}{12}$	$\frac{60}{9}$	5.2	$\frac{61}{12}$	$\frac{56}{13}$	$\frac{54}{25}$
$\frac{62}{25}$	$\frac{62}{11}$	$\frac{70}{9}$	7.2	$\frac{79}{12}$	$\frac{68}{15}$	$\frac{63}{25}$	
$\frac{80}{25}$	$\frac{85}{11}$	$\frac{91}{10}$	$\frac{85}{8}$	8.4	$\frac{88}{12}$	$\frac{98}{14}$	$\frac{88}{25}$
$\frac{36}{25}$	$\frac{48}{10}$	$\frac{48}{8}$	$\frac{52}{6}$	5.0	$\frac{55}{16}$	$\frac{44}{19}$	$\frac{48}{25}$
	$\frac{41}{25}$	$\frac{53}{9}$	$\frac{73}{6}$	6.7	$\frac{60}{8}$	$\frac{66}{16}$	$\frac{53}{18}$
	$\frac{60}{25-17}$	$\frac{78}{7}$	$\frac{105}{3}$	$\frac{86}{2}$	7.6	$\frac{84}{17}$	$\frac{69}{20-25}$
	$\frac{82}{25-14}$	$\frac{93}{8}$	$\frac{120}{4}$	10.8	$\frac{103}{9}$	$\frac{110}{16}$	$\frac{84}{19-25}$
	$\frac{50}{25}$	$\frac{50}{10}$	$\frac{67}{5}$	6.8	$\frac{62}{7}$	$\frac{68}{13}$	$\frac{52}{17}$
	$\frac{65}{25}$	$\frac{66}{9}$	$\frac{81}{5}$	7.8	$\frac{79}{7}$		$\frac{74}{25}$
	$\frac{86}{25}$	$\frac{86}{7}$	$\frac{93}{5}$	$\frac{86}{3}$	8.0	$\frac{85}{3}$	$\frac{82}{9}$
					$\frac{86}{18}$	$\frac{79}{20-25}$	

Spike E root 15" Maple 25 Lt ± Sta 20+15

$\frac{7.4}{15}$	$\frac{61 \text{ in Channel}}{7}$	4.8	$\frac{50}{16}$	$\frac{55}{18}$	$\frac{47}{19}$	$\frac{35}{25}$
$\frac{5.2}{25}$	$\frac{47}{2}$	5.2	$\frac{50}{15}$	$\frac{54}{17}$	$\frac{34}{21}$	$\frac{24}{25}$

		1273.60		
21+0			3.8	69.8
	√86	1277.57	1.95	1271.65
22+0			5.2	75.3
22+1.8			3.23	1274.28
			0.34	1277.17
	300	1277.28		
23+0			6.4	70.9
24+0			6.1	71.2
25+0	408	1274.80	6.56	1270.72
			4.5	70.3
26+0			6.3	68.5
27+0			8.0	66.8
28+0			9.2	65.6
	345	1268.89	9.36	1265.44
28+76	Culvert			
29+0			4.5	64.4
30+0			4.1	64.8
BM#4			0.42	1268.47

1268.59

	$\frac{60}{25}$	$\frac{50}{15}$	$\frac{40}{7}$	$\frac{50}{6}$	$\frac{40}{4}$	38	$\frac{35}{5}$	$\frac{40}{3}$	$\frac{26}{11}$	$\frac{16}{25}$
	$\frac{74}{25}$	$\frac{61}{8}$	$\frac{63}{6}$	$\frac{54}{5}$	5.2	$\frac{49}{4}$	$\frac{53}{11}$	$\frac{59}{13}$	$\frac{49}{16}$	$\frac{39}{25}$
	on boulder } top nearest iron F. Post }									
	$\frac{64}{25}$	$\frac{64}{12}$	$\frac{70}{6}$	64	$\frac{70}{14}$	$\frac{60}{16}$	$\frac{50}{25}$			
	25	$\frac{61}{9}$	$\frac{72}{8}$	$\frac{65}{6}$	61	$\frac{65}{12}$	13.5	$\frac{67}{19}$	$\frac{55}{19}$	$\frac{50}{25}$
	25	$\frac{57}{10}$	$\frac{54}{7}$	$\frac{46}{6}$	4.5	$\frac{46}{11}$	$\frac{52}{13}$	$\frac{41}{15}$	$\frac{36}{25}$	
	25	$\frac{60}{10}$	$\frac{72}{8}$	$\frac{66}{7}$	63	$\frac{67}{10}$	$\frac{71}{11}$	$\frac{53}{15}$	$\frac{44}{25}$	
	25	$\frac{82}{12}$	$\frac{86}{10}$	$\frac{86}{6}$	80	$\frac{81}{10}$	$\frac{85}{11}$	$\frac{66}{13}$	$\frac{54}{25}$	
		$\frac{104}{25}$	$\frac{100}{8}$	9.2	$\frac{88}{9}$	$\frac{96}{11}$	$\frac{80}{15}$	$\frac{75}{25}$		
	$\frac{97}{100}$	$\frac{78}{60}$	$\frac{64}{FL}$	$\frac{57}{Top P.}$		$\frac{50}{Top P.}$	$\frac{62}{FL}$	$\frac{78}{60}$	$\frac{97}{100}$	
	$\frac{58}{25}$	$\frac{51}{14}$	$\frac{57}{12}$	$\frac{50}{10}$	4.5	$\frac{46}{6}$	$\frac{50}{8}$	$\frac{38}{11}$	$\frac{28}{25}$	
	$\frac{65}{25}$	$\frac{58}{20}$	$\frac{55}{10}$	$\frac{50}{5}$	4.1	$\frac{48}{10}$	$\frac{36}{12}$	$\frac{36}{18-25}$		Fd 11/1/50

Spike Wood 24 Maple 25 Rte Sta 30+10

31+0		1268.89	3.4	65.5	
32+0	259	1267.29	4.9	1264.70	
33+0			7.0	60.3	
34+0 = culvert	571	1264.07	8.93	1258.36	
35+0			6.5	57.6	
36+0			4.8	59.3	
37+0			4.6	59.5	
38+0	834	1272.41	0.00	1264.07	
39+0			6.8	65.6	
40+0			5.4	67.0	
40+0			9.98	1262.43	1262.55
40+25			13.5	58.9	
41+0	659	1267.65	11.35	1261.06	
42+0			7.0	60.7	
			<del>4.2</del>	<del>63.5</del>	
			4.2	63.5	

	$\frac{5.3}{25}$	$\frac{3.2}{5}$	$\frac{3.9}{3}$	3.4	$\frac{3.4}{12}$	$\frac{1.9}{18}$	$\frac{0.9}{25}$		
	$\frac{4.4}{25-20}$	$\frac{3.5}{12}$	$\frac{4.2}{6}$	$\frac{4.6}{5}$	4.4	$\frac{4.2}{10}$	$\frac{4.7}{13}$	$\frac{2.8}{16}$	$\frac{1.9}{25}$
	$\frac{7.5}{25}$	$\frac{6.5}{15}$	$\frac{7.9}{12}$	7.0	$\frac{7.3}{5}$	$\frac{5.3}{8}$	$\frac{3.8}{25}$		
	T.P. on Rock Outcrop at Sta							33+80	
	$\frac{12.9}{25}$	$\frac{12.5}{FL}$	$\frac{10.4}{Top Pipe}$	6.5		$\frac{8.6}{FL Pipe}$	$\frac{10.5}{FL}$	$\frac{9.1}{20}$	
	$\frac{4.9}{25}$	$\frac{5.6}{15}$	$\frac{4.6}{5}$	4.8	$\frac{5.2}{2}$	$\frac{3.5}{4}$	$\frac{1.2}{25}$		
	$\frac{6.4}{25}$	$\frac{5.9}{17}$	$\frac{6.3}{15}$	$\frac{5.3}{11}$	4.6	$\frac{4.9}{6}$	$\frac{5.5}{8}$	$\frac{4.9}{10}$	$\frac{3.4}{25}$
		$\frac{3.4}{13}$	$\frac{3.9}{10}$	3.2	$\frac{3.4}{8}$	$\frac{3.7}{10}$	$\frac{2.6}{12}$	$\frac{1.6}{25}$	
	$\frac{7.1}{25}$	$\frac{6.8}{10}$	$\frac{7.7}{8}$	6.8	$\frac{7.3}{12}$	$\frac{5.4}{15}$	$\frac{5.2}{25}$		
	$\frac{4.9}{20}$	$\frac{4.6}{5}$	$\frac{5.8}{3}$	5.4	$\frac{5.3}{16}$	$\frac{3.9}{19}$	$\frac{3.8}{25}$		
	Spike Wroot 30 Maple 30 RT at Sta							39+90	No Find
	$\frac{16.0}{25}$			13.5	$\frac{12.3}{3}$	$\frac{12.2}{17}$	$\frac{13.1}{25}$	1/11/50	
	$\frac{17.5}{25} FL$	$\frac{16.4}{FL Pipe}$			$\frac{14.4}{Top Pipe}$	$\frac{15.6}{FL}$	$\frac{14.3}{30}$		
	$\frac{8.6}{25}$	$\frac{8.6}{12}$		7.0	$\frac{7.1}{18}$	$\frac{6.9}{25}$			
	$\frac{3.9}{25-16}$	$\frac{3.2}{5}$	$\frac{4.2}{3}$	4.2	$\frac{3.7}{4}$	$\frac{4.2}{13}$	$\frac{1.5}{18}$	$\frac{0.7}{25}$	



125825

54			7.7	50.6	
	3.95	1257.70	4.50	1253.75	
54+56	coln.		7.0	50.7	

55			6.7	51.0	
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56			5.6	52.1	
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57			4.5	53.2	
B4#7	1.81	1257.68	1.81	1255.89	1255.87

58			4.1	53.6	
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58+11	plot section		4.2	53.5	
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57+97	coln.				
<del>58+</del>					

59			2.9	54.8	
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	6.42	1261.15	2.95	1254.73	
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60			5.5	55.7	
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61			4.7	56.5	
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62			4.8	56.4	
----	--	--	-----	------	--

—	$\frac{25}{9.1}$	$\frac{15}{9.0}$	$\frac{10}{8.7}$	$\frac{7}{7.9}$	$\frac{25}{5.2}$	—	—
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$\frac{150}{12.4}$	$\frac{50}{10.4}$	$\frac{FI}{10.3}$	$\frac{10}{8.8}$	$\frac{70}{8.6}$	$\frac{FI}{10.2}$	$\frac{25}{8.9}$
--------------------	-------------------	-------------------	------------------	------------------	-------------------	------------------

—	$\frac{25}{8.4}$	$\frac{11}{7.7}$	$\frac{7}{7.2}$	$\frac{6}{7.0}$	$\frac{9}{8.2}$	$\frac{13}{7.6}$	$\frac{25}{7.0}$
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$\frac{25}{6.6}$	$\frac{15}{6.4}$	$\frac{11}{7.0}$	$\frac{8}{6.3}$	$\frac{9}{6.1}$	$\frac{10}{7.0}$	$\frac{12}{6.0}$	$\frac{25}{4.7}$
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—	$\frac{25}{6.0}$	$\frac{10}{5.7}$	$\frac{6}{5.2}$	$\frac{10}{4.9}$	$\frac{15}{5.9}$	$\frac{16}{4.8}$	$\frac{25}{4.2}$
---	------------------	------------------	-----------------	------------------	------------------	------------------	------------------

Spike E root 2" Maple 30' R/L 57+85 Fd 1/11/50

$\frac{100}{8.5}$	$\frac{25}{5.5}$	$\frac{25}{2.8}$	$\frac{100}{0.3}$
-------------------	------------------	------------------	-------------------

$\frac{70}{4.6}$	$\frac{FI}{5.9}$
------------------	------------------

—	—	$\frac{25}{3.8}$	$\frac{10}{4.0}$	$\frac{16}{3.2}$	$\frac{17}{4.0}$	$\frac{20}{3.3}$	$\frac{25}{2.3}$
---	---	------------------	------------------	------------------	------------------	------------------	------------------

—	—	$\frac{25}{6.8}$	$\frac{13}{6.6}$	$\frac{9}{5.4}$	$\frac{15}{6.5}$	$\frac{12}{4.0}$	$\frac{25}{3.5}$
---	---	------------------	------------------	-----------------	------------------	------------------	------------------

$\frac{25}{5.9}$	$\frac{12}{5.7}$	$\frac{10}{6.1}$	$\frac{7}{5.5}$	$\frac{9}{4.7}$	$\frac{14}{5.7}$	$\frac{16}{4.5}$	$\frac{25}{3.8}$
------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------

$\frac{25}{6.1}$	$\frac{13}{5.6}$	$\frac{11}{6.4}$	$\frac{8}{5.6}$	$\frac{9}{5.1}$	$\frac{14}{6.0}$	$\frac{18}{3.9}$	$\frac{25}{3.4}$
------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------

1261.15

BM#8		2.90	1258.25
63		5.1	56.1
64		4.8	56.4
64+17	Colva		
65		4.1	57.1
	3.81	1261.59	3.37
			1257.78
66		3.7	57.9
67		3.8	57.8
68		4.2	57.4
69		5.2	56.4
BM#9		5.96	1255.63
70		6.4	55.2
71		7.0	54.6
72		5.9	55.7
	3.27	1258.76	6.10
			1255.49

Spike NE root 10" Ash 25' H ± Sta 61+97

$\frac{25}{70}$	$\frac{14}{63}$	$\frac{11}{67}$	$\frac{8}{59}$	$\frac{9}{55}$	$\frac{14}{65}$	$\frac{16}{54}$	$\frac{25}{46}$
$\frac{25}{72}$	$\frac{19}{69}$	$\frac{14}{71}$	$\frac{7}{52}$	$\frac{7}{48}$	$\frac{13}{68}$	$\frac{18}{46}$	$\frac{25}{52}$
$\frac{100}{89}$	$\frac{F1}{80}$	$\frac{70}{64}$		$\frac{70}{57}$	$\frac{F1}{71}$		
$\frac{29}{47}$	$\frac{13}{47}$	$\frac{10}{52}$	$\frac{8}{46}$	$\frac{11}{44}$	$\frac{14}{52}$	$\frac{17}{39}$	$\frac{25}{34}$
$\frac{25-13}{45}$	$\frac{10}{48}$	$\frac{8}{41}$		$\frac{11}{40}$	$\frac{13}{46}$	$\frac{16}{33}$	$\frac{25}{30}$
$\frac{25-14}{49}$	$\frac{11}{51}$	$\frac{8}{45}$		$\frac{9}{46}$	$\frac{13}{50}$	$\frac{16}{36}$	$\frac{25}{31}$
$\frac{25-12}{49}$	$\frac{10}{53}$	$\frac{9}{49}$		$\frac{11}{44}$	$\frac{13}{54}$	$\frac{16}{41}$	$\frac{25}{37}$
$\frac{25-12}{57}$	$\frac{10}{65}$	$\frac{8}{60}$		$\frac{9}{53}$	$\frac{13}{65}$	$\frac{17}{49}$	$\frac{25}{45}$

Spike NW root 15" Apple 25' H ± Sta 69+60 Gone

$\frac{25}{76}$	$\frac{13}{74}$	$\frac{11}{76}$	$\frac{7}{69}$	$\frac{10}{67}$	$\frac{13}{73}$	$\frac{18}{65}$	$\frac{25}{59}$
$\frac{25-13}{69}$	$\frac{10}{79}$	$\frac{6}{72}$		$\frac{12}{70}$	$\frac{15}{80}$	$\frac{18}{69}$	$\frac{25}{66}$
$\frac{25-15}{67}$	$\frac{12}{76}$	$\frac{8}{64}$		$\frac{10}{64}$	$\frac{13}{73}$	$\frac{17}{63}$	$\frac{25}{60}$

125876

73		3.9	54.9
74		5.5	53.3
75		5.1	53.7
75+19	culv.	4.9	53.9
76		5.8	53.0
77		5.6	53.2
78		3.8	55.0
	7.16 126288	3.04	1255.72
79		5.3	57.6
BM #10		3.46	1259.42
80		4.7	58.2
81		4.8	58.1
82		5.5	57.4
82+84	culv.		

$$\frac{25-15}{43} \frac{12}{5.7} \frac{8}{4.4} \quad \frac{9}{4.1} \frac{14}{5.2} \frac{19}{5.2} \frac{25}{3.0}$$

$$\frac{25-18}{53} \frac{12}{7.0} \frac{8}{5.9} \quad \frac{9}{5.9} \frac{14}{6.6} \frac{20}{5.5} \frac{25}{5.3}$$

$$\frac{25-19}{71} \frac{13}{7.9} \frac{7}{5.2} \quad \frac{9}{5.2} \frac{16}{7.8} \frac{18}{7.2} \frac{25}{7.0}$$

$$\frac{50}{10.2} \frac{F1}{9.1} \frac{70}{6.1} \frac{H}{3.5} \quad \frac{H}{3.5} \frac{70}{6.2} \frac{F1}{9.0} \text{ ---}$$

$$\frac{25-16}{74} \frac{12}{7.9} \frac{7}{6.1} \quad \frac{11}{6.1} \frac{16}{7.7} \frac{22}{7.0} \text{ ---}$$

$$\frac{25-14}{66} \frac{10}{7.0} \frac{5}{5.8} \quad \frac{11}{5.6} \frac{16}{7.1} \frac{22}{6.9} \text{ ---}$$

$$\frac{25}{30} \frac{15}{3.7} \frac{10}{5.1} \frac{6}{4.3} \quad \frac{12}{4.1} \frac{17}{5.2} \frac{22}{4.6} \frac{25}{7.6}$$

$$\frac{25-15}{53} \frac{9}{6.7} \frac{5}{5.6} \quad \frac{11}{5.6} \frac{16}{6.8} \frac{20}{5.3} \frac{25}{4.6} \text{ fd}$$

Spike W. root 18' Maple 30' Rd 5/2 79+40 1/11 50

$$\frac{25-15}{5.5} \frac{10}{6.2} \frac{6}{4.9} \quad \frac{13}{5.1} \frac{15}{5.3} \frac{18}{4.9} \frac{25}{\text{---}}$$

$$\frac{25-13}{5.5} \frac{10-8}{6.2} \frac{6}{5.0} \quad \frac{12}{5.1} \frac{16}{5.4} \frac{18}{4.7} \frac{25}{3.9}$$

$$\frac{25-14}{6.5} \frac{11}{7.1} \frac{6}{5.7} \quad \frac{14}{6.2} \frac{25}{4.7} \text{ --- ---}$$

$$\text{---} \frac{100}{8.9} \frac{F1}{7.7} \frac{70}{7.2} \quad \frac{70}{6.6} \frac{F1}{7.3} \text{ --- ---}$$

126288

83 58 57.1

84 4.8 58.1

2.82 126087 4.83 1258.05

85 3.5 57.4

86 4.7 56.2

87 4.4 56.5

87+13 Culv.

88 3.9 57.0

89 2.4 58.5

7.75 126624 2.38 1258.49

89+23 Culv. 7.4 58.8

90 7.1 59.1

91 6.2 60.0

92 4.6 61.6

9.67 127340 2.51 1263.73

$$\frac{25}{73} \frac{9}{72} \frac{6}{61} \quad \frac{13}{57} \frac{16}{68} \frac{18}{62} \frac{25}{57}$$

$$\frac{25}{58} \frac{16}{59} \frac{11}{50} \frac{7}{50} \quad \frac{10}{51} \frac{13}{55} \frac{15}{46} \frac{25}{40}$$

$$\frac{25}{38} \frac{16}{50} \frac{11}{40} \frac{7}{40} \quad \frac{9}{39} \frac{12}{47} \frac{15}{33} \frac{25}{26}$$

$$\frac{25}{44} \frac{14}{48} \frac{11}{60} \frac{7}{50} \quad \frac{11}{49} \frac{14}{61} \frac{16}{47} \frac{25}{41}$$

$$\frac{25}{56} \frac{14}{64} \frac{11}{48} \frac{7}{48} \quad \frac{9}{48} \frac{14}{64} \frac{20}{67} \frac{23}{64}$$

clean 200 Lt.  $\frac{100}{70} \frac{F1}{73} \frac{70}{61}$

$$\frac{70}{67} \frac{H}{74}$$

$$\frac{25}{49} \frac{15}{61} \frac{12}{45} \frac{7}{45} \quad \frac{11}{44} \frac{16}{51} \frac{25}{38} \quad \text{---}$$

$$\frac{25}{40} \frac{16}{46} \frac{11}{28} \frac{7}{28} \quad \frac{9}{28} \frac{14}{43} \frac{17}{35} \frac{25}{25}$$

$$\frac{100}{10.8} \frac{F1}{10.2} \frac{70}{86} \frac{H}{6.2} \quad \frac{H}{64} \frac{70}{8.8} \frac{F1}{10.2}$$

$$\frac{25}{83} \frac{18}{90} \frac{13}{74} \frac{9}{74} \quad \frac{8}{75} \frac{14}{90} \frac{20}{78} \frac{25}{73}$$

$$\frac{25}{72} \frac{20}{81} \frac{14}{64} \frac{7}{64} \quad \frac{7}{66} \frac{13}{84} \frac{20}{66} \frac{25}{67}$$

$$\frac{25}{61} \frac{20}{69} \frac{15}{52} \frac{10}{52} \quad \frac{8}{48} \frac{12}{69} \frac{20}{50} \frac{25}{47}$$

Shaw 5' ditch from 9 H50 south to Culvert on RL

127340

BM #11		6.52	1266.88
93		7.6	65.8
94		4.8	68.6
95		3.8	69.6
	8.24	1277.99	3.65
96		6.3	71.7
96+68	← Road	3.7	1274.3
BM #12		4.17	1273.82
98		3.7	74.3
99		2.5	75.5

Spiko SE root 24" Maple 35' Lt & Sta 92+60

$\frac{25}{50}$	$\frac{18}{54}$	$\frac{13}{38}$	$\frac{8}{7.8}$	$\frac{8}{8.2}$	$\frac{16}{10.1}$	$\frac{21-25}{70}$
$\frac{25}{50}$	$\frac{16}{52}$	$\frac{13}{64}$	$\frac{9}{5.1}$	$\frac{7}{5.1}$	$\frac{13-14}{7.1}$	$\frac{19-25}{48}$ $\frac{25}{46}$
$\frac{29}{5.1}$	$\frac{17}{49}$	$\frac{14}{57}$	$\frac{8}{4.2}$	$\frac{9}{3.8}$	$\frac{14-15}{5.2}$	$\frac{18-}{36}$ —
—	—	$\frac{25}{6.9}$	$\frac{11}{70}$	$\frac{7}{6.4}$	$\frac{16}{7.3}$	$\frac{22}{3.1}$ $\frac{25}{4.4}$
		$\frac{100}{5.7}$	$\frac{25}{4.2}$	$\frac{25}{3.3}$	$\frac{50}{2.8}$	$\frac{100}{2.0}$

X out SE & S Headwall 15' RT &

— —

Check Level on Downings Cor Rd.

BM #12	4.17	1277.99	1	1273.82	
	2.12	1271.18	8.93	1269.06	
BM #11			4.30	✓	1266.88
	1.95	1261.78	11.35	1259.83	
	5.24	1262.37	4.65	1257.13	
BM #10			2.98	1259.37	1259.42
	0.66	1258.08	4.95	1257.42	
	4.57	1260.07	<sup>2.78</sup> 2.58	1255.50	
BM #9			4.38	1255.69	1255.63
	3.52	1261.35	2.24	1257.83	
BM #8			3.10	1258.25	1258.25
	2.56	1259.10	4.81	1256.54	
BM #7			3.23	✓	1255.87





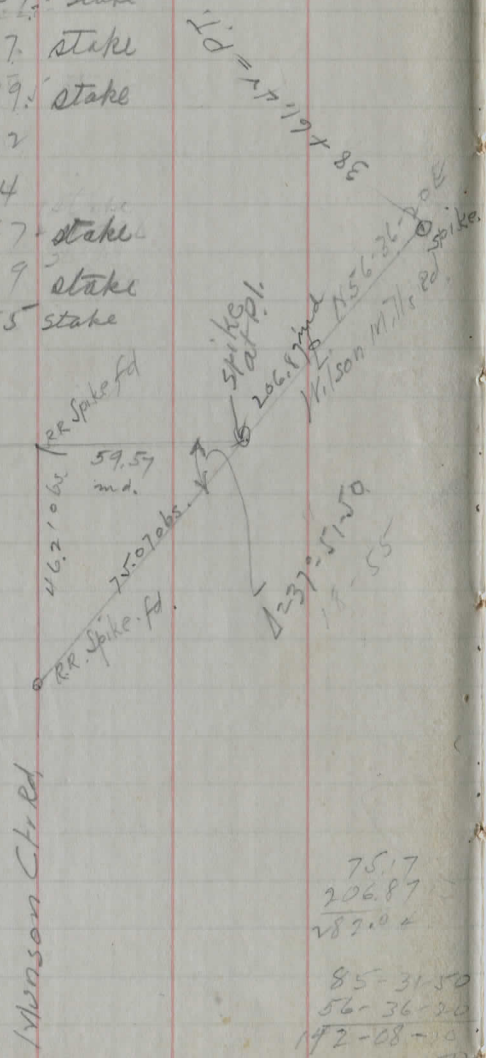


8-8-39 N. Line Wilsons Mills Rd.  
 Graber  
 Richards  
 Drey  
 Claus

- 38+61.42 0-0 stake
- 38+50 0-32
- 38+0 2-54.5 stake
- 37+50 5-17 stake
- 37+0 7-39.5 stake
- 36+50 10-02
- 36+0 12-24
- 35+50 14-47 stake
- 35- 17-09 stake
- 34+62.85 18-55 stake

34+62.85=PC

85-31-50E



Id = 1719 + 85

Wilson Creek

36+10.15  
 1.47.30  
 ---  
 34+62.85  
 3+98.57  
 ---  
 38+61.42

75.17  
 206.87  
 ---  
 282.04  
  
 85-31-50  
 56-36-20  
 ---  
 192-08-30  
 37-51-50

100' = 425' .0475  
 11.42  
 ---  
 1900  
 475  
 ---  
 475  
 ---  
 1541.50  
 60  
 ---  
 32.46

37.1

# Location Curve at Dunning's Corner

$\Delta = 52^\circ 25'$

$D = 20'$

B Curve Data  $T = 140.96$

$E = 32.8$

$L = 262.08$

PC = 90+78.89

PT = 93+40.97

$R = 286.4P$

SE Corner  
of Intersection

90+74 = 0° 00'  
91+00 = 2° 06'  
91+50 = 7° 06'  
92+00 = 12° 36'  
92+50 = 17° 06'  
93+00 = 22° 06'  
93+41 = 26° 12'

so chords = 49.94

Sta 22+19.85 PI Def Rt  $52^\circ 25'$  Set

$\Delta = 37^\circ 51' 50''$

$D = 9^\circ 30'$

$T = 206.87$

$E =$

$L = 398.57$

PC  $1+00.00$

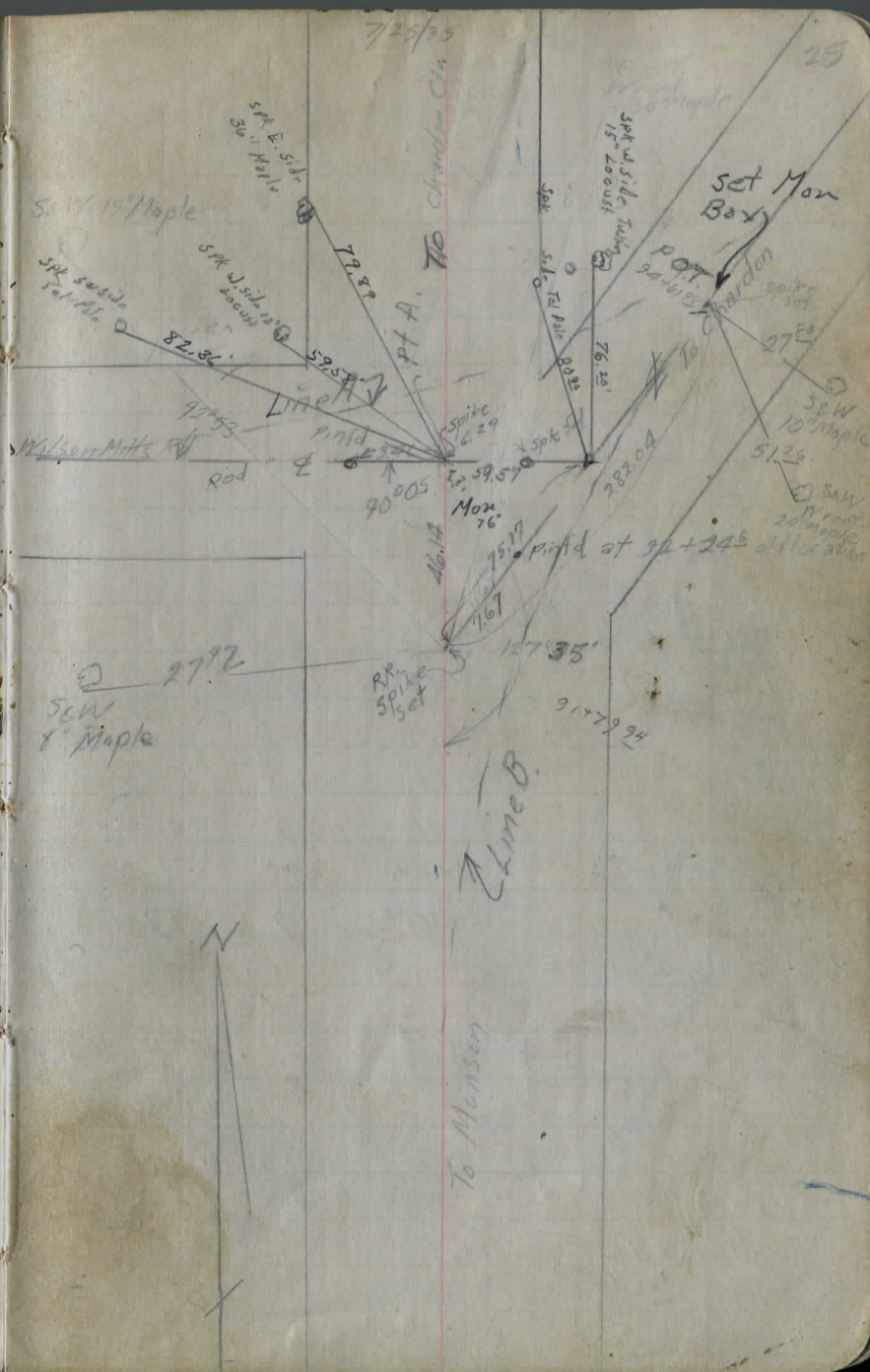
PT  $4+98.57$

$R = 603.12$

A Curve  
Data  
Northside  
of Intersection

1+50 = 2-22-  
2+00 = 4-45  
2+50 = 7-07  
3+00 = 9-30  
3+50 = 11-52  
4+00 = 14-15  
4+50 = 16-37  
4+ =  
4+ =

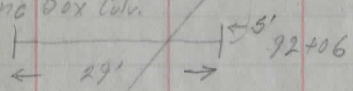
so chords = 49.99



Topography Line B

Original notes  
 Culvert at 92+03 on tangent  
 15.0' Lt. 10'2" Rt. ← Extended later

Anchor	16	93+42		
T	21	93+42		
		93+35	26	Ø 12" M
30" M Ø	21	93+21		
		92+50	23	Anchor
		92+45	9'	T C&G
		92+38	17	Ø 18" Wa
Cone Extension 4' on East end 2 x 1/2 Cone Box Culv.				
		91+52	18	T
Drive		91+55		
T C&G	23'	91+28		



BM #1 1313.24  
 + 3.43  
 HI = 1316.67  
 - 5.24  
 New BM #1 = 1311.43

→ Spike S.W. root 30" Maple 100' Rt Sta 1+00  
 and 160' NE of Sta 0+00.

Notes for Court Case.

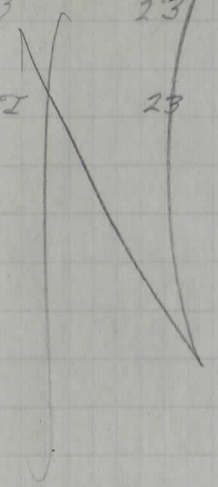
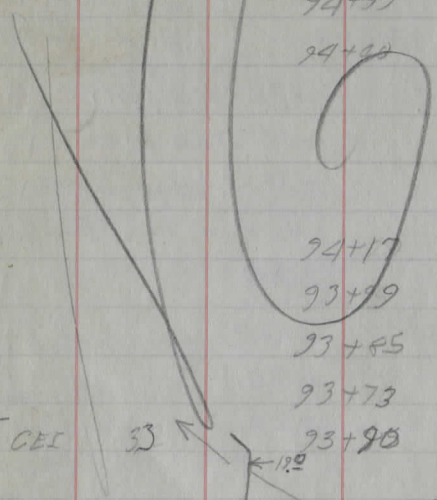
	H.I.	615   40
6.70	1318.13	see H. Hill
		1311.13 BM.
		(S.S. side)
0+00	-7.2	FL, Culv. 1310.9
0+00	-3.8	Top H Wall 1314.3
+2.	-5.1	S edge Berm 1313.0
0+13	-4.64	" " Pavc 13135
0+33	3.60	1314.5
0+50	2.20	1315.9
+56	1.90	1316.2
+65	2.20	1315.9

FL = 2.1 below berm at culvert  
 Berm 11 ft. wide " "  
 Pavc 20 " wide " "  
 1:20 = 5% grade (across paving)

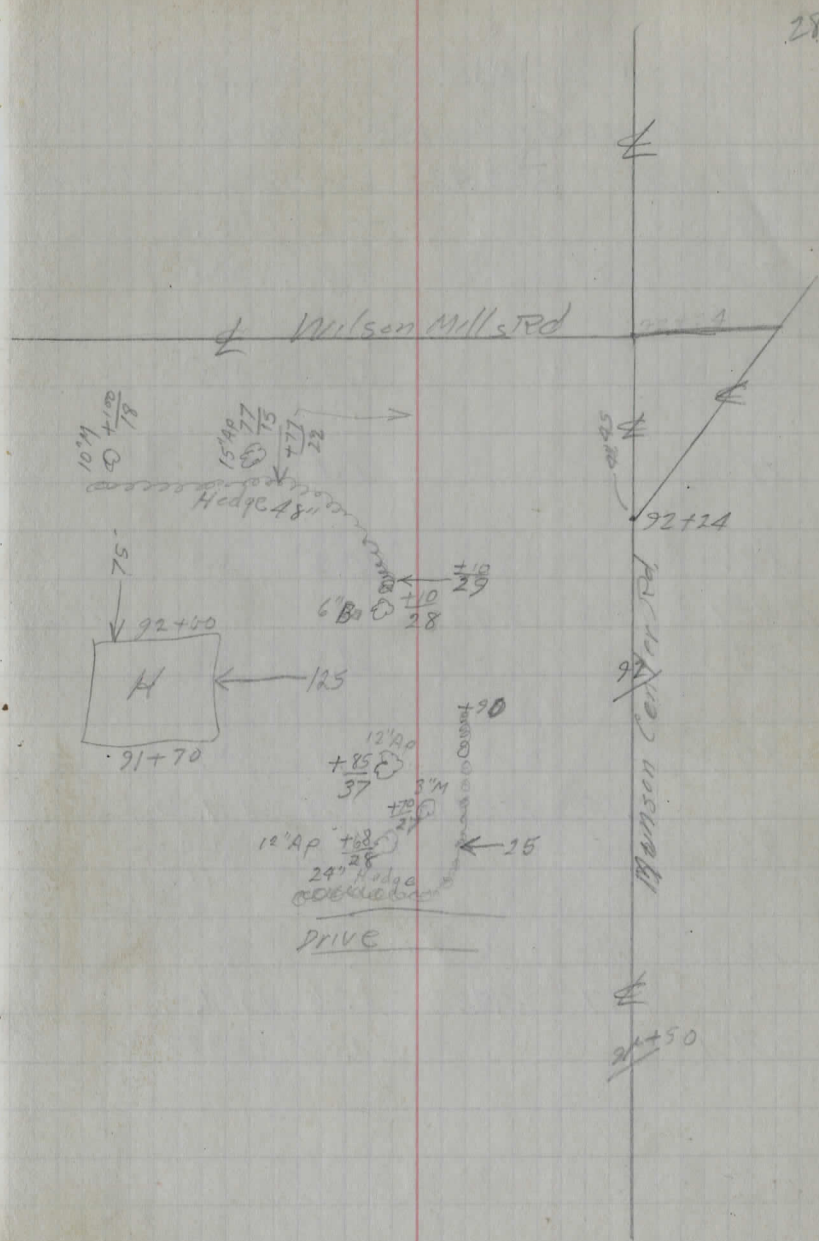
Topography Line A.

		95+90	23	30" WC
T	20	95+86		
12" Wa	18	95+62		
CEI T	26	95+35		
		95+25	20	24" M
		94+25	22	6" Ap.
		94+80	26	8" M.
4" Lo	25	94+65		
T	20	94+47		
		94+55	28	10" M
		94+40	27	12" M
		94+26		
		94+20		
		94+17	25	18" M
		93+99	24	18" M
		93+85		DRIVE
		93+73	20	10" M
T CEI	33	93+90		
		93+75		
12" CIP Culv. Hillside Roadwalks				
30° Skew				
		93+13	6'	12" M

Anchor	16	92+28		
18" Wa	19	92+20		
T CEI	27	92+26		
T	17	91+50		
12" Ap	23	90+25		
		89+82	22	T
T CEI	23	89+75		
		89+15	27	4" M
		89+00		DRIVE



Topography on Tangent at Sta 92+24  
Downings Corners



	+	H.I.	-	Elev
	Cross Sections Line A			
BM#1	1018	1323.42		1313.24
88			-0.2	23.2
89			1.9	21.5
90			3.7	19.7
91			7.1	16.3
92			10.5	12.9
BM#1	1.04	1314.28		1313.24
93			4.5	89.8
94			9.5	84.8
95	2.20	1301.10	12.38	1301.90
			6.2	94.9
96			13.8	87.2
	12.37	1314.27	2.20	1301.90
BM#1			1.03	1313.24 ✓

✓ B.M. Moved See page 26  
 Spike W root 36" Maple 100' NE of Sta 92+25

$\frac{25}{1.2}$	$\frac{16}{1.6}$	$\frac{11}{3.9}$	$\frac{6}{21}$	$\frac{13}{21}$	$\frac{17}{32}$	$\frac{20}{21}$	$\frac{25}{14}$
------------------	------------------	------------------	----------------	-----------------	-----------------	-----------------	-----------------

$-\frac{18}{29}$	$\frac{13}{58}$	$\frac{10}{38}$	$\frac{12}{3.8}$	$\frac{15}{57}$	$\frac{20}{34}$	$\frac{25}{43}$
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$\frac{38}{60}$	$\frac{33}{77}$	$\frac{30}{60}$	$\frac{16}{6.0}$	$\frac{9}{8.1}$	$\frac{5}{7.0}$	$\frac{25}{8.2}$	—	—	—
-----------------	-----------------	-----------------	------------------	-----------------	-----------------	------------------	---	---	---

$\frac{45}{88}$	$\frac{42-41}{11.2}$	$\frac{37}{78}$	$\frac{28}{85}$	$\frac{25}{11.3}$	—	—	—
-----------------	----------------------	-----------------	-----------------	-------------------	---	---	---

$\frac{35}{48}$	$\frac{32}{42}$	$\frac{22}{39}$	$\frac{11}{43}$	$\frac{65}{73}$	$\frac{3}{4.4}$	$\frac{25}{4.9}$	—	—	—
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------	---	---	---

$-\frac{23}{94}$	$\frac{19}{108}$	$\frac{14}{100}$	$\frac{9}{9.9}$	$\frac{14}{10.6}$	$\frac{24}{7.0}$	$\frac{10:1}{10:1}$
------------------	------------------	------------------	-----------------	-------------------	------------------	---------------------

$-\frac{23}{26}$	$\frac{14-13}{73}$	$\frac{11}{64}$	$\frac{11}{6.6}$	$\frac{14}{81}$	$\frac{22}{19}$	$\frac{27}{24}$
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10/10/1911

10/10/1911

Cross Sections Line B

BM#1 1018 1323.42 1313.24

91+00 6.0 17.4

91+50 6.4 17.0

92+00 9.7 13.7

92+06 Colu.

92+50 10.0 13.4

BM#1 104 1314.28 1317.24

93 2.8 11.5

93+21 on Line B = 93+00 on Line A

BM moved see page 26

25 14 9 6 14 12 23 30  
5.5 6.7 8.7 6.1 6.3 8.5 7.2 8.9

25 16 14 12 8 13 15 25  
6.2 6.8 7.9 6.4 6.6 8.6 7.6 8.7

42 38 35 32 7 2 2 10 11 25  
6.7 9.1 7.8 7.3 7.6 9.8 8.2 8.5 9.1 9.6

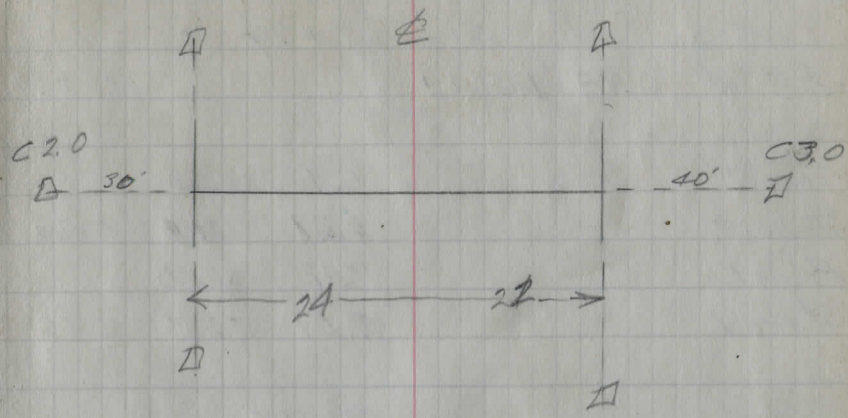
F1 T0 T4 T4 T0 F1  
9.7 8.5 6.3 6.6 9.1 10.4

50 20 25 6-7 11 25  
9.5 9.0 10.5 12.7 9.1 9.8

20 13-15 11 1.3 1.7 2.3 25-  
0.6 4.1 3.6 3.2 6.3 1.7 2.8

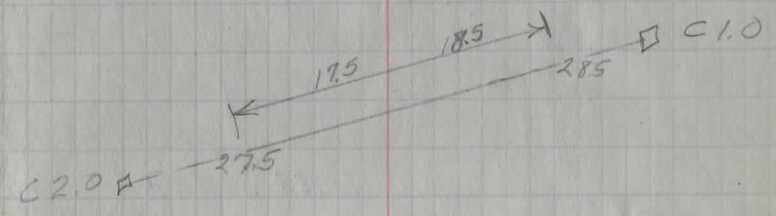
No. 6 Culvert at Sta 49+49

BM	1.28	1259.61		1257.73
	4.98	1256.94	7.05	1251.96
Flow R			9.94	1247.0
Stake R			9.64	6.64 C 3.0
Flow L			12.44	1244.5
Stake L			12.70	10.70 C 2.0



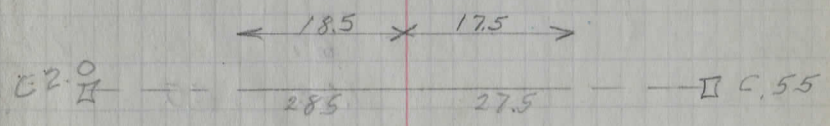
No. 1 Sta 8+86

BM# 2	3.85	1289.36		1285.51
±		1289.24		
Flow R			6.36	1283.0
Stake R			6.51	5.51 C 1.0
Flow L			5.86	1283.5
Stake L			5.71	3.71 C 2.0

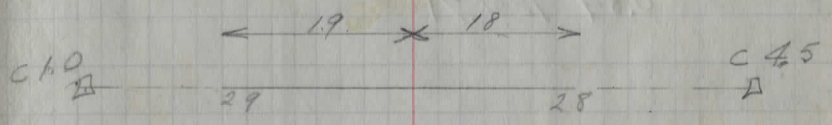


No. 2 Sta 20+15

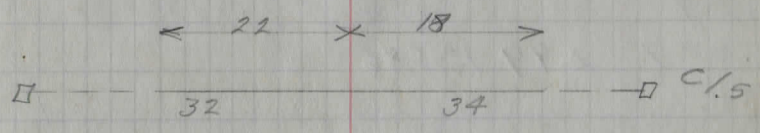
BM# 3	6.08	1273.98		1267.90
±		1268.98		
Flow R			6.98	1267.0
Stake R			6.83	1.33 C 5.5
Flow L			7.48	1266.5
Stake L			7.63	5.63 C 2.0



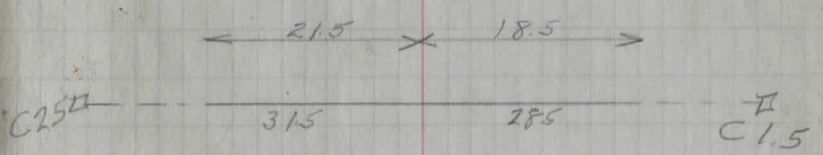
No. 3  
 BM#4 0.83 1269.42 1268.59  
 1265.0  
 Flow R 6.92 1262.5  
 Stake R 6.77 2.27 C 4.5  
 Flow L 7.42 1262.00  
 Stake L 7.57 6.57 C 1.0



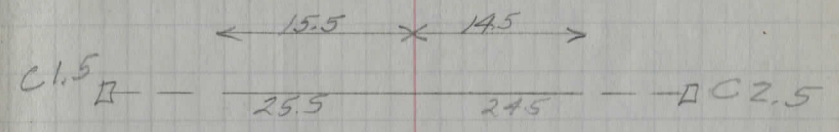
No 4  
 BM#4 1.35 1269.94 1268.59  
 2.52 1273.43 9.03 1270.91  
 Flow R 8.63 1254.8  
 Stake R 7.63 6.13 C 1.5  
 Flow L 12.13 1251.3  
 Stake L 13.13 11.63 C 1.5



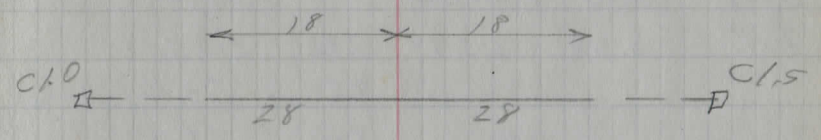
No 5  
 BM#5 1.90 1264.45 1262.55  
 1261.0  
 Flow R 7.45 1257.0  
 Stake R 6.65 5.15 C 1.5  
 Flow L 9.75 1254.7  
 Stake L 10.55 8.05 C 2.5



No 8 Sta 54+<sup>65</sup>~~56~~  
 BM# 7 0.84 1256.71 1255.87  
 ± 12510  
 Flow R 8.71 1248.0  
 Stake R 8.41 ~~5.91~~ C2.5  
 Flow L 9.71 1247.0  
 Stake L 10.01 8.51 C1.5

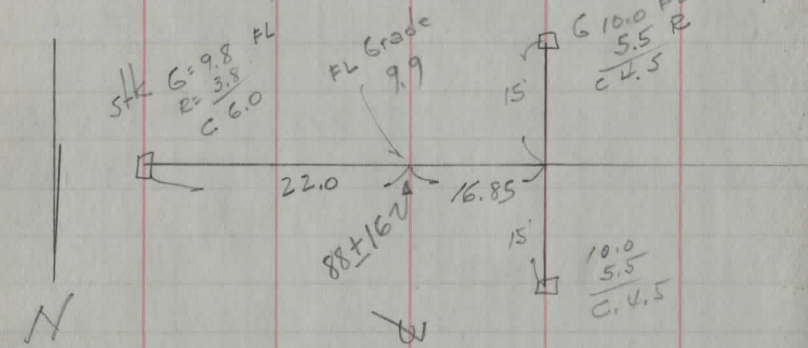


No 9 Sta 57+97  
 BM# 7 2.99 1258.86 1255.87  
 Flow R 10.5 1252.2  
 Stake R 5.90 4.40 C1.5  
 Flow L 1250.8  
 Stake L 9.00 8.00 C1.0



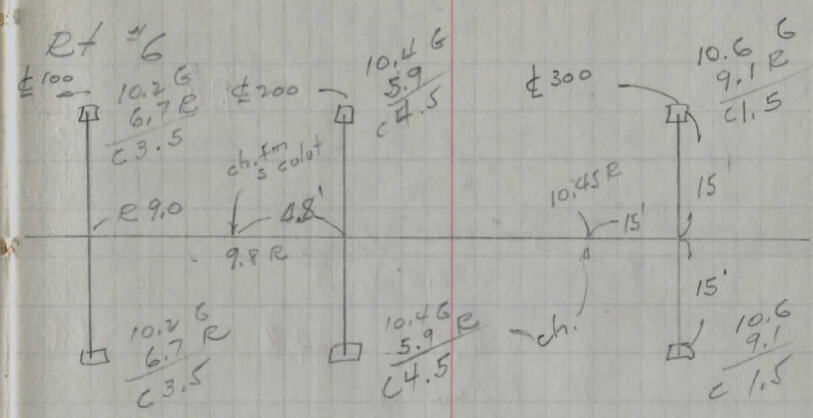
5/12/50

No 4 Sec ① New culvt ± 600' S of



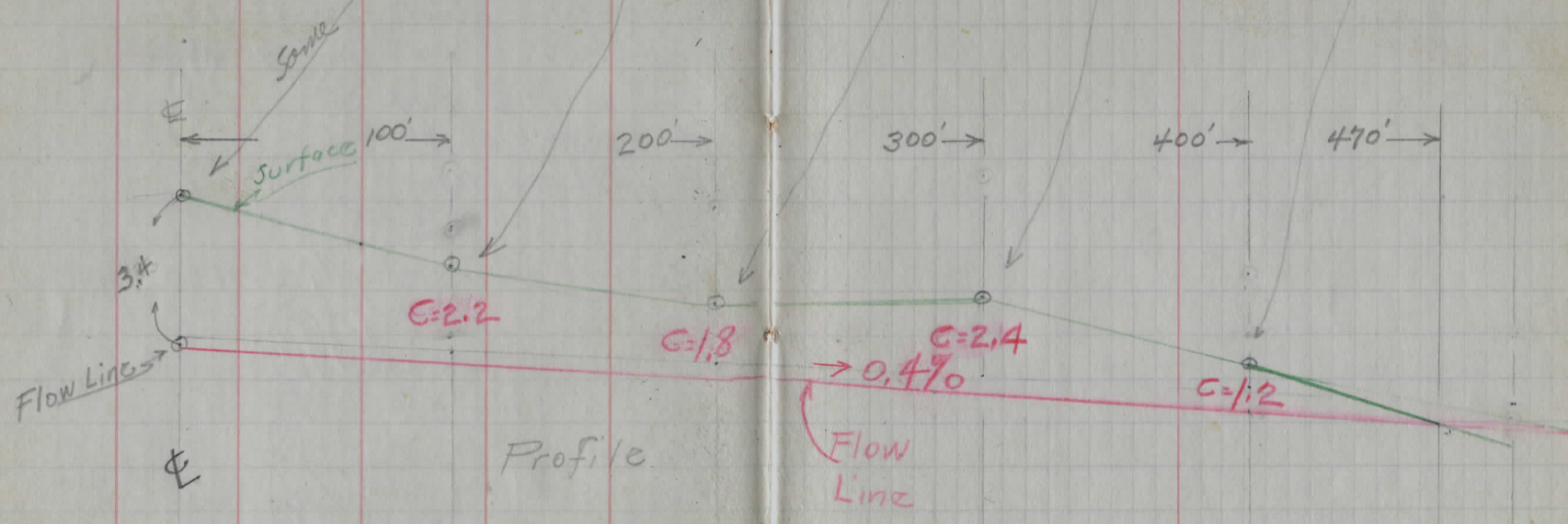
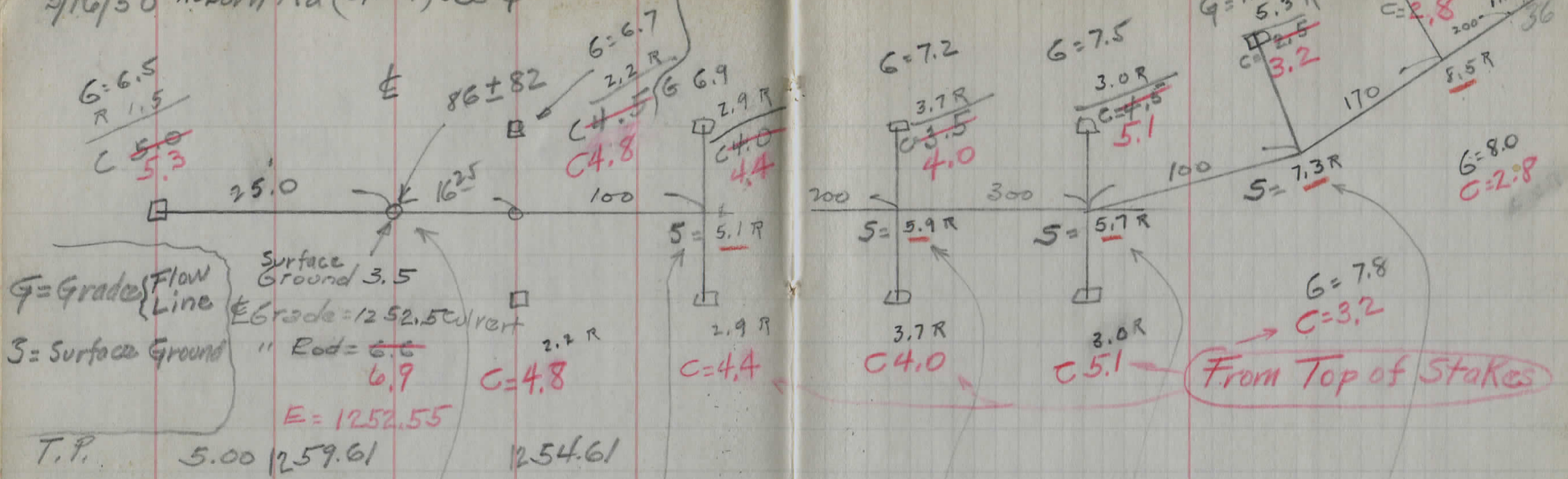
B.M.	3.10	62.55	1259.45
T.P.	8.58	63.19	7.94
			54.61
			9.8
			53.4 (53.6)
			8.0
			55.2
			10.45
			6.0
			7.20
			7.8
			11.1
			10.9
			11.2
			9.9
			9.6
			13.0
			11.5
			11.6
			15.3
			47.9

See next pg



- EXISTING
- Outlet FL culvt Sta 87+13
  - " " " " 89+24
  - 300' W of E Sta 88+16
  - E Sta 88+16
  - E ditch 88+16
  - W " " "
  - 350 W in exist ch ± N 85° W fm 300'
  - 400 " " " "
  - 60' SW of 300' splc
  - 160' " " " "
  - 140 " " " "
  - 166 " " " "
  - 200 " " " "
  - 250 " " " "
  - 280' " " " "
- Long hole
- Main valley E side

5/16/50 Auburn Rd (CH #4) Sec Q









7/30/35

40

Location Munson Center South Rd.

← 32 3

✓

x

4/

x

24" A @ +30  
30  
✓

+10 T  
23

✓

x

N40°40'E

SEW  
6" Locust

95' L

0/

Sta 0-42<sup>75</sup>

POT

spike  
set

26' 89

SEW  
15" Maple

1900' T

spike  
set

← 30 →

pipe & S Line  
Spaulding term

Sta 8+00

± Mayfield Rd

Spike set

S&W 15" Maple

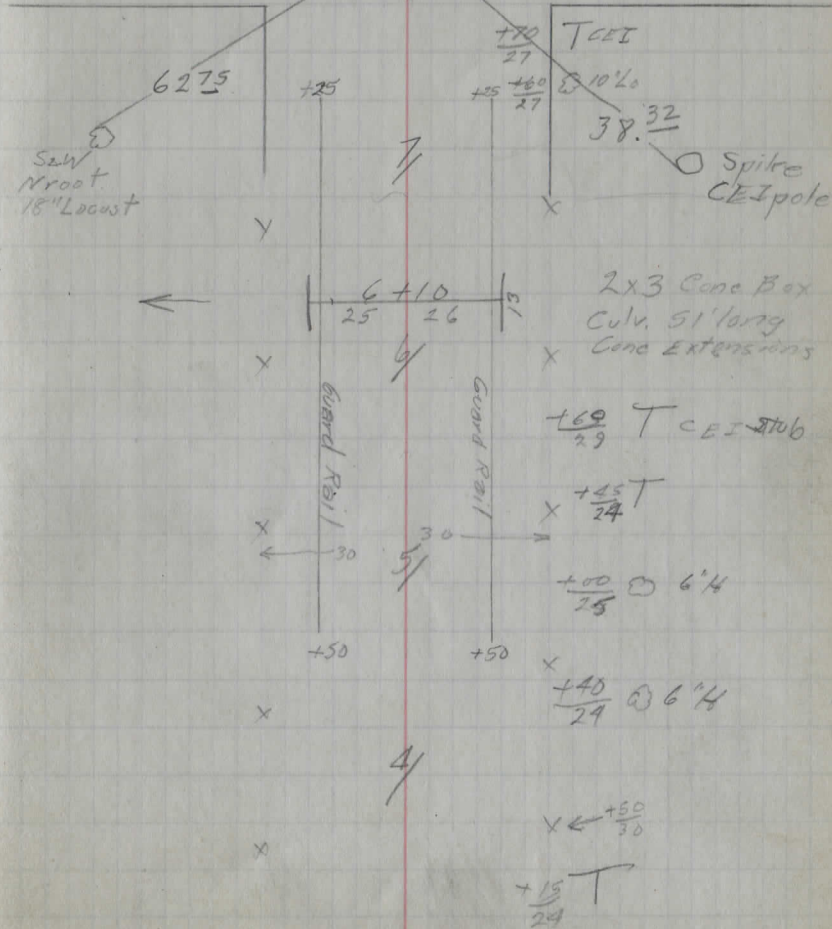
43.60

39'±

5/22/103

Pg. 56 this book

Mayfield Rd





Cross Sections			Monson Center S. Rd.		
BM# 1	1.36	1240.91			1239.55
264			6.2	34.7	12344
8			3.3	37.6	
7+50			5.2	35.7	
7			7.4	1233.5	
	2.13	1236.74	6.30	1234.61	
6+10	Colv.				
6			4.6	32.1	
5			2.4	34.3	
	12.18	1247.44	1.48	1235.26	
4			8.6	38.8	
	12.26	1258.90	0.80	1246.64	
3			12.1	46.8	
2+65			8.5	50.4	
2			3.4	55.5	
	11.75	127037	0.28	1258.62	

SE 4<sup>th</sup> 1<sup>st</sup> step 40' NE of Sta 8+00

		$\frac{25}{50}$	$\frac{25}{7.6}$		
	$\frac{31}{47}$	$\frac{25}{82}$	$\frac{19}{63}$	$\frac{12}{53}$	$\frac{19}{98}$ $\frac{34}{08}$
	$\frac{29}{10.6}$	$\frac{22}{12.7}$	$\frac{11}{8.0}$	$\frac{12}{81}$	$\frac{21}{13.0}$ $\frac{33}{73}$
	$\frac{F1}{15.4}$	$\frac{T0}{13.4}$	$\frac{T4}{10.8}$	$\frac{T4}{10.7}$	$\frac{T0}{13.1}$ $\frac{F1}{16.1}$
	$\frac{32}{13.8}$	$\frac{8}{4.7}$		$\frac{8}{4.8}$	$\frac{27}{14.4}$
	$\frac{30}{6.0}$	$\frac{30}{6.3}$	$\frac{11}{2.6}$	$\frac{9}{2.7}$	$\frac{21}{7.6}$ $\frac{31}{8.8}$
	$\frac{33}{10.0}$	$\frac{16}{9.2}$	$\frac{10}{8.8}$	$\frac{9}{8.8}$	$\frac{16}{10.6}$ $\frac{22}{11.1}$ $\frac{32}{12.1}$
	$\frac{30}{4.4}$	$\frac{17}{13.0}$	$\frac{11}{11.6}$	$\frac{10}{12.4}$	$\frac{24}{13.8}$
	$\frac{30}{7.3}$	$\frac{15}{9.6}$	$\frac{11}{8.0}$	$\frac{11}{9.0}$	$\frac{18}{11.1}$ $\frac{31}{1.5}$
	$\frac{28}{-3.5}$	$\frac{16}{4.9}$	$\frac{12}{3.3}$	$\frac{12}{3.9}$	$\frac{15}{5.3}$ $\frac{30}{-2.5}$

		1270.37		
1			7.4	63.0
	7.56	1275.66	2.27	1268.10
0			7.2	68.5
0-100			3.9	71.8
BM #3			3.46	1272.20

check level

	3.46	1275.66		1272.20
	0.83	1266.27	10.22	1265.44
	0.12	1254.65	11.74	1254.53
	2.03	1244.26	12.42	1242.23
	6.47	1241.06	9.67	1234.59
BM #1			1.52	1237.54 1237.55
	1.52	1241.07		
BM #2			5.18	1235.89

$$\frac{-26}{4.7} \quad \frac{16}{25} \quad \frac{13}{7.9} \quad \frac{10}{8.1} \quad \frac{16}{9.2} \quad \frac{29-}{2.4}$$

$$\frac{-15}{3.7} \quad \frac{13}{8.3} \quad \frac{10}{7.0} \quad \frac{11}{7.3} \quad \frac{14}{7.0} \quad \frac{27-}{2.7}$$

$$\frac{-19}{4.4} \quad \frac{14}{5.1} \quad \frac{2}{4.0} \quad \frac{12}{4.2} \quad \frac{15}{5.3} \quad \frac{30}{5.4}$$

Spike W. root 15" Maple 25' RH ± Sta 0-42

Reference S2W N root 18" Locust 40' LH ± Sta 7+70

Cross Sections for borrow pit

BM #1 13.40 125295 123955

0+50 1460 Tel pole 29' RT

1470 CEI pole 29' RT

1+00 15' M 2+10 25' RT

1+50 same type as 2+00 15' M 2+60 29' RT

2+00

10.82 1262.41 236 125059

3+00

12' M 2+85 25' RT

CEI pole 3+05 29' RT

-0.01 1251.42 10.00 1251.41

BM #1 11.92 1239.50 1239.55

Station on R.R. 4.2 1237.7 1237.5

0+50

1+00

0 = Mayfield Rd  $\frac{1}{2}$  to East  
Sections Taken parallel with Munson Cir Rd. <sup>South</sup>

$\frac{5}{12.3}$   $\frac{12}{12.4}$   $\frac{16}{13.0}$   $\frac{19}{10.8}$   $\frac{30}{10.0}$   $\frac{45}{10.0}$   $\frac{85}{14.0}$  —

$\frac{5}{8.9}$   $\frac{15}{10.0}$   $\frac{20}{6.0}$   $\frac{50}{6.3}$   $\frac{100}{10.3}$   $\frac{131}{13.8}$

$\frac{5}{2.7}$   $\frac{18}{3.0}$   $\frac{20}{1.5}$   $\frac{70}{3.1}$   $\frac{100}{4.1}$   $\frac{135}{4.8}$   $\frac{200}{2.6}$

$\frac{5}{5.9}$   $\frac{18}{6.4}$   $\frac{21}{4.7}$   $\frac{70}{5.9}$   $\frac{100}{5.2}$   $\frac{155}{4.5}$   $\frac{200}{4.7}$   $\frac{250}{6.0}$

$\frac{100}{1.2}$   $\frac{115}{4.2}$   $\frac{140}{11.5}$   $\frac{158}{2.0}$   $\frac{170}{5.5}$

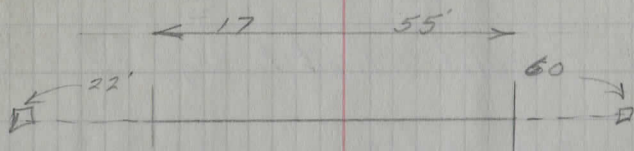
4/19/57

46

## Levels on Culvert at 92+03

E Pt.	4.3		
E edge	5.3		
Flow Lt	7.5		
Stake Lt	7.3	3.3	C4.0
Flow Rt	9.3		
Stake Rt.	9.5	7.0	C2.5

1.7

1.0  
2.5

+

-

Elev. BM

Inside 1<sup>st</sup> culvert hdwall to edge rd. = 10'

	+	-	Elev.	BM
B.M	5.39	1318.63		1313.24
Hillside Hdwl	0.0	9.0	1309.6	
Edge part	3 $\frac{1}{2}$ '	10.1	1308.5	
Crown	12 $\frac{1}{2}$	9.9	1308.7	
Far edge part	22	10.8	1307.8	

0+30 100' Rt. Downings Cors North Rd

4.5% Grade. around Curve.

Sec. 135' West of Hillside H.W.

0	ditch	6.9	1311.7
12 $\frac{1}{2}$		4.0	1314.6
22		3.6	1315.0
33		2.9	1315.7
50		2.0	1316.6

{ 4.0% crown. } 5.5%

Munson TWP

Bean Rd 1

E. Cushing

Cleve-Meadville

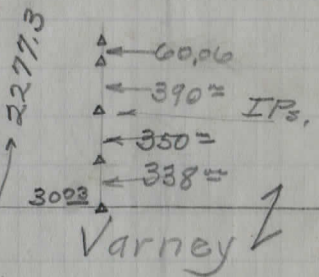
See pg 40

Spaulding

Klatka

Friel

Notes hereon  
C. Peterson correlated  
various surveys



F. Gibson

Varney

A. Summers

Δ to Left ?

Spk. NW. side  
8" Apple

E. Colvin

Weidlein

Spk. E. side  
16" Locust

A. Davey Tr.

Perry Brown

Spk. S. root 10" Maple

Spk. 1st 10"  
Maple W. of  
drive

Spk. N.E.  
Side 10"  
Twin Locust

Spk. S.W.  
CEI pole

I.P.

109-02-30

4087

SPK  
I.P.

179-53

90-13-30?

2590

90-00

Bean Rd.

8-26-46  
Pom  
Thrasher  
Nojard

# Alignment & drainage structures CHARDON-

7+0

29' □

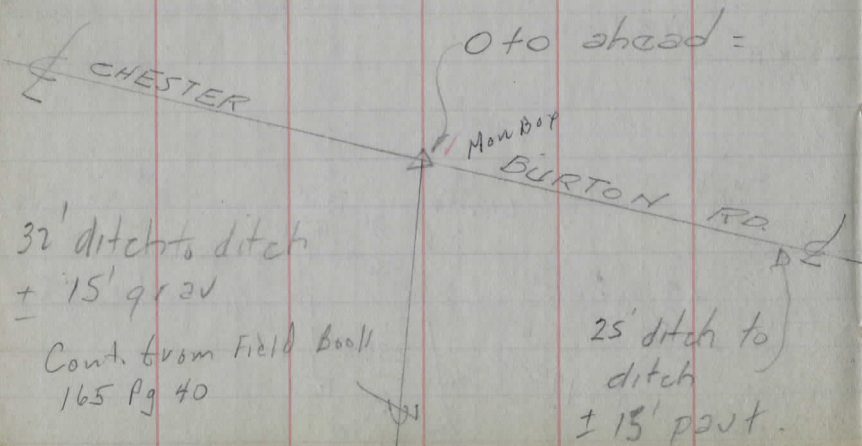
2+81<sup>2</sup>

12" x 31' Conc. pipe OK  
Relay for grade

A=

D=

R=



0+0 ahead =

78+67<sup>00</sup> back

Iron rod fd  
See ref.

18" under  
Fd. bk. #165 pg 40

NOTE: Stakes set 30' Rt  
unless otherwise indicated

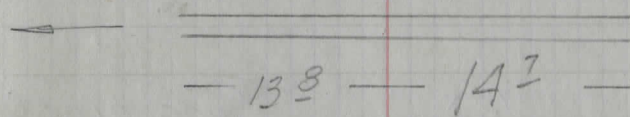
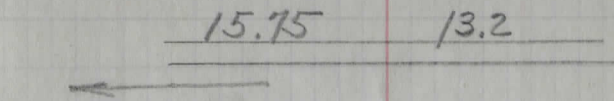
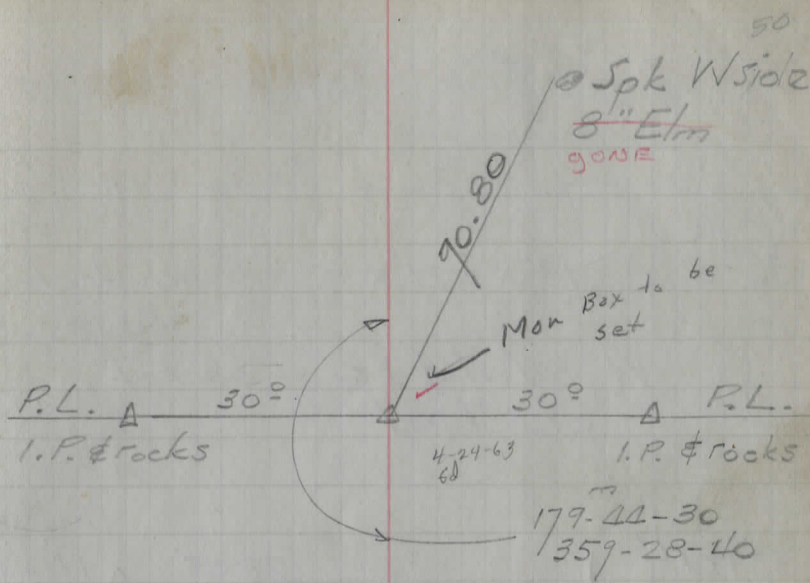
# AUBURN (N<sup>o</sup> 1 SEC'S L & M)



16+96.70  $\Delta = 0-15-40$  I.P. Fd. 8" under

12+60 15" x 30" cone OK.  
E ditch higher than rd.

9+27<sup>8</sup> 12" x Conc. pipe OK



36 to 18" x ± 21" x Conc. Arch  
cut

W hdwl ± 6' of barrel  
cracked

33 to 1<sup>77</sup>

29.85

Peterson  
I.P. + d  
Gibson

26 to P.O. T. I.P. set

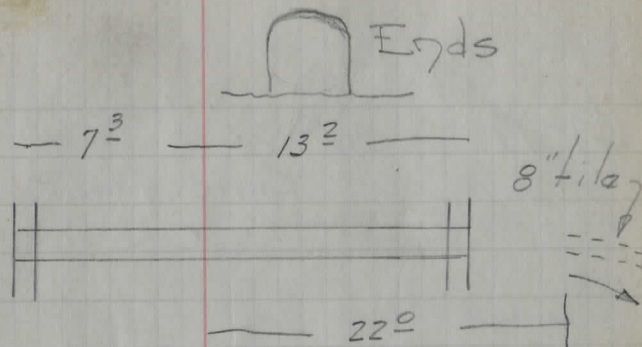
17 to 83<sup>8</sup>

12" x

Conc. pipe  
OK

Relay

51.

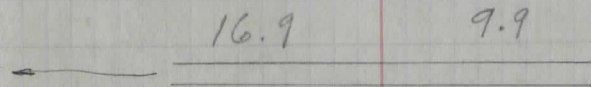


Spk SW root  
~~36" Elm~~  
gone

Spk S side 85.60  
~~24" Mulberry~~  
gone

27<sup>88</sup>  
Ed. 4-24-63

Spk S side  
CEI  
# 192801



49+99

30" x 26 1/2" Conc. box  
Conc. floor  
OK

46+87 1/2

12" Conc. pipe  
and (W) length undermined

46+70 85

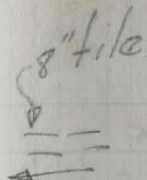
34 90

I.P. Fd

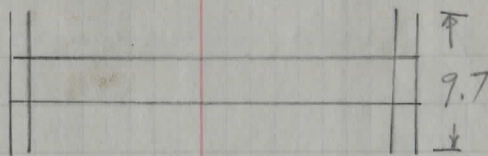
Δ

42+0 P.O.T.

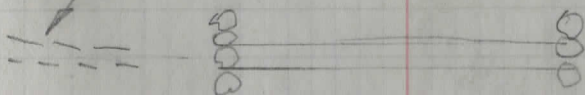
I.P. Set



← 13.9 → 14.1 →

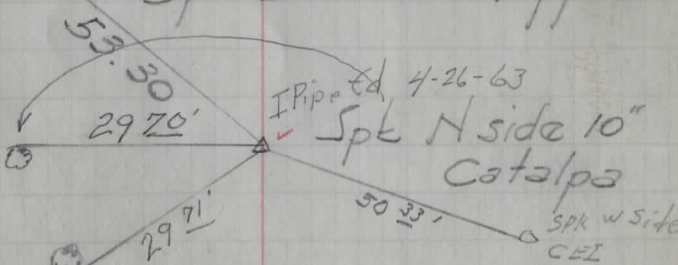


10" tile | 15° — 17.7 |

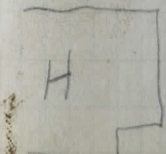


| 23° —

Gone Spk E side 15" Apple



Bent Spk N side 40" Maple root



70+32.9 18" X

Conc. pipe  
OK

58+04.78 P.O.T.

I.P. Set

66+0



30°

53+0



30°

R.T.  
179-46

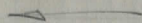
52+98.15



I.P. Fd.

17.9

14.7



I.P.

30°

Man Box to be set

30°

I.P.

+d 4-24-63

90°

79.85

Spk W side 45" Ash

House

Spk S side Cor Fence post

Man Box to be set

I.P. set

± 90°

30+0

+d 4-24-63

36.68

52.65

2' ditch to d

BEAM RD. ± 10' gravel

15" Cast Iron (Pipes)

43.83

Spk W side Cor fence Post

Spk W side 8" Loc.

88+96

30°  $\Delta$  I.P.  
Fd

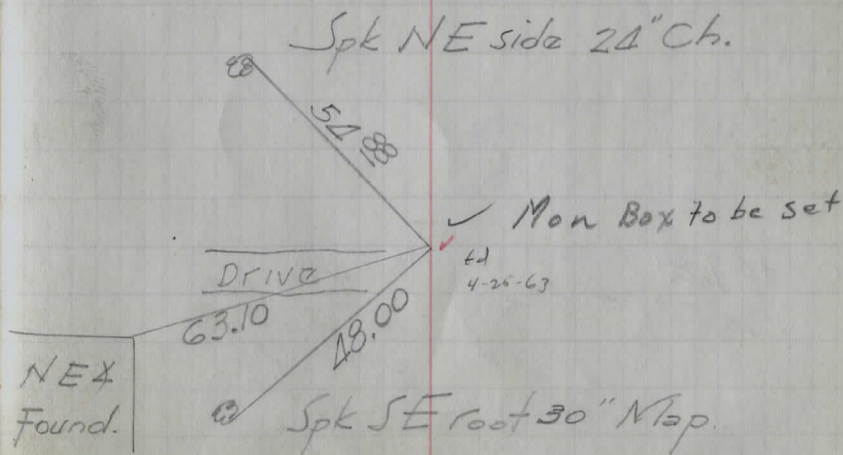
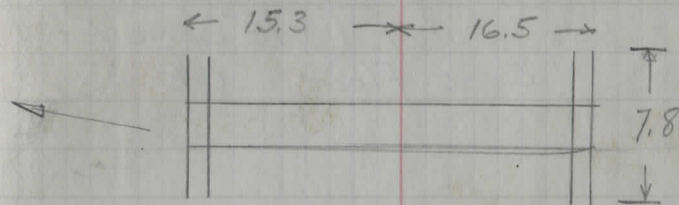
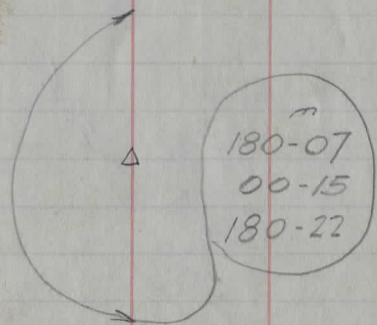
P.L.

81+29<sup>2</sup> 2' x 1 1/2' x 32' Stone & Conc  
Box (Stone ctr &  $\pm$  5' conc. ext.  
both ends) OK  
Conc. floor

76+16<sup>3</sup>

30°  $\Delta$  I.P.  
Fd.

72+22<sup>56</sup>  
I.P. set



97+0

25' □

96+98<sup>0</sup>

Stone & conc  
box culvert (+18' conc Rt &  
Conc. floor OK

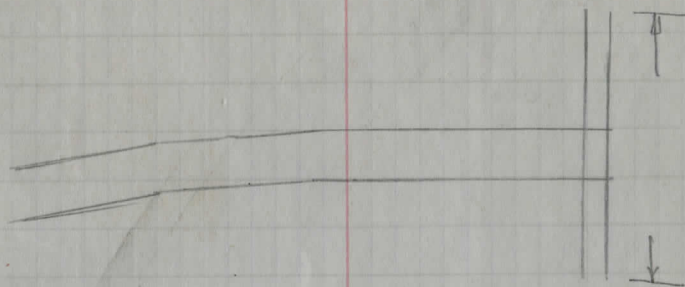
94+40<sup>5</sup>

30<sup>10</sup> △  
I.P. Fd

32<sup>11</sup>

90 +67.89

26<sup>5</sup> →



Spk NE side  
11" Loc

611

Min Box to be set  
I. Pin

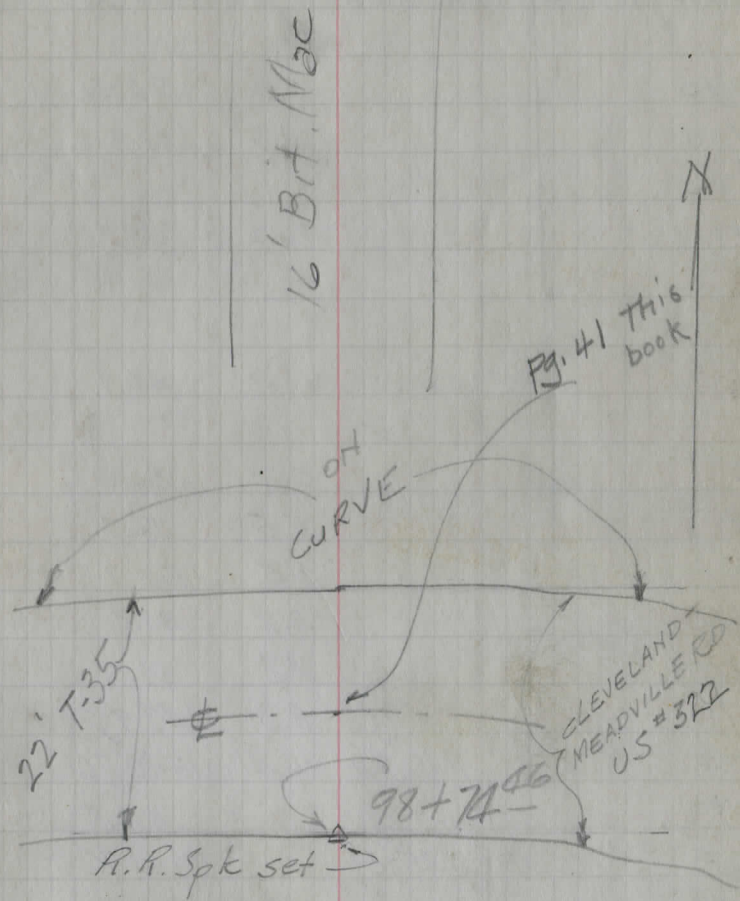
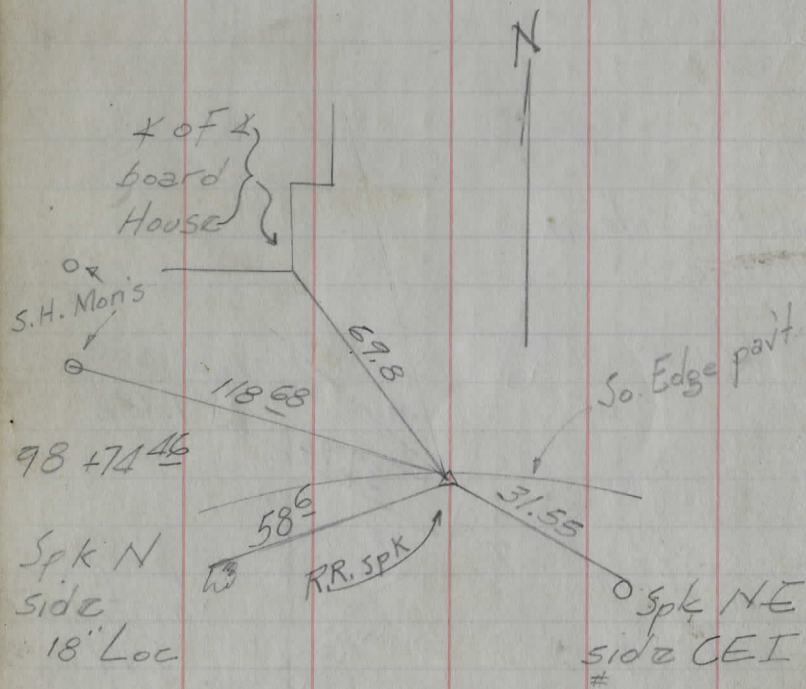
37.92

I.P. Set P.O.T.

td 4-25-63

38.0

Vert. Spk  
S.W.  
root  
18" Map.



CHARDON-AUBURN RD

8-30-46

Pan Thrasher Maynard

2 A.M.

B.M. 1 1.39 1156.17 ✓ 1354.78

0 to 3.9 52.3

1 4.9 51.3

2 49.8

17.9

8.3

30

+82 culvt 49.9

3 6.2 50.0

4 5.5 50.7

5 3.5 52.7

+50 3.2 53.0

6 4.2 52.0

7 8.3 47.9 ✓

T.P. 4.53 1149.29 ✓ 11.41 1344.76

8 44.8

T.P. 0.33 1145.09 ✓ 1344.76

9 2.0 43.1

culvt 42.8

10 2.6 42.5

11 4.6 40.5

12 5.9 39.2

13 6.3 38.8

No 4 Sec L-M

57

Ref. Spk W side Map. NE quad. of X

0 to

W

E

49.3

48.9

48.5

49.0

49.9

49.6

49.0

49.2

50.8

50.2

50.3

6.9 7.3 7.7 7.2 6.4 6.3 6.6 7.2 7.0 5.4 6.0 5.9  
20.5 15 12 10.5 6 1.5 7 12.5 14.5 18 22 30

10.2

6.3

8.3

FL

FL

42.9

42.7

43.8

43.6

43.9

44.4

46.7

6.4 6.6 5.5 5.7 4.5 5.4 4.9 2.6  
30 23 14.5 11 1 11.5 20 25

6.0

2.3

4.7

FL

FL

✓  
1345.09

14		✓	5.8	39.3	
T.P.	0.28	1339.47	5.90	1339.19	
15		-0.02	1.7	37.7	
B.M. 2		<u>1339.45</u>	2.19	1337.28	26

16 31.1

17 7.2 32.2

+ 84 culot

18		✓	7.8	31.6	
T.P.	7.56	1339.55	7.68	1331.79	77
19		33	7.0	32.3	

20 5.6 33.7

21 4.8 34.5

22

23 0.9 38.4

T.P.	9.23	1348.47	0.39	1338.96	
24		1348.17	8.0	94	40.1
25		-0.06	6.0		42.1

26 4.9 43.2

27 4.2 43.9

B.M. 3		✓	2.44	1345.75	
28				67	44.0

29 4.4 43.7

Spk E side 14" Hick 22' W Sta. 15 ± 55

33.8	34.3	33.0	33.8	33.6	33.1	34.8	35.8	
5.6	5.1	6.4	5.6	5.3	5.8	6.3	4.6	3.6
30	17.5	14	6.5		8	13.5	17	30
	24.5							

		31.7	
11.2		7.7	10.1
FL			FL

34.1	35.6	36.1	35.7	35.6	36.6	38.0
5.2	3.7	3.2	3.6	3.7	2.7	1.3
30	5		7	12.5	16	30

Ref Spk S.W. side 28" Elm ± 25' W

44.6	43.8	Sta. 26 + 96			
3.5	4.3	4.1	4.4	4.9	5.3
30	8.5		9.5	16	30
			43.7	43.2	42.8

✓  
1348.19  
11

W

E

30		✓	5.2	42.9
T.P.	1.23	1344.04	5.38	1342.81
31		1343.96	2.4	41.6
32			3.5	40.5
33			4.3	39.7
34			5.0	39.0
35			5.8	38.2

36		✓		38.3
T.P.	5.05	1342.67	6.42	1337.62
		.59		.54

7.9	5.0	5.7	5.5	8.3
FL	Hdwl		Hdwl	FL

→

37				37.5
----	--	--	--	------

5.3	5.7	6.3	5.8	5.1	5.3	6.6	5.6	5.1
30	13.5	12	9	2	9	16.5	18.5	30

38			4.8	37.8
39			4.7	37.9
40			4.2	38.4
41			2.4	40.2

T.P.	2.01	1344.55	0.13	1342.54
42		.47	1.7	.46
43	Quit 8-30-16		4.3	40.2
B.M.4			6.01	1338.54
				.46

Spk SE root 18" Maple 25' West  
Sta 43 ± 73

2-3-48  
J. Maynard +  
F.C.P.

CHECK-BACK

BM 4	8.55	1347.09		1338.54
T.P.	6.14	1344.13	9.10	1337.99
T.P.	5.20	1348.35	0.98	1343.15
BM 3			2.60	1345.75 1345.75
TP	.80	1339.39	9.76	1338.59
BM 2	6.56	1343.95	2.00	1337.39 1337.78
T.P.	7.56	1349.47	2.04	134.91
T.P.	6.54	1355.74	0.27	1349.20
BM #1			0.80	1354.94 1354.78

BM #4	4.45	1342.99		1338.54
T.P.	0.25	1332.10	11.14	1331.85
T.P.	9.35	1333.10	8.35	1323.75
T.P.	10.00	1343.10	0.00	1333.10
B.M. #5			1.39	1341.71

3.88 a20

2-18-48 Maynard \* Randles Rd

B.M.		0.88	1261.44	1261.16
T.P.	12.38	1262.32	1.86	1249.94
T.P.	12.14	1251.80	1.24	1239.66
98+85				38.3
B.M.	40.70	3.88	1237.02	
BM		9.20	31.70	
98	2.4			35.1
97		1240.90		33.2

use  
1338.46

Spk SE root 18" Map. pg 59

use  
1345.67  
pg 58

use  
1337.26  
pg 58

use  
1354.78  
pg 57

61.48  
16  
32

pg 59 1338.46

Spk W side 18" Ash 1st N of Cushing Drive

Pam - Notes 11:15 AM  
S.E. cor. Mine House (porch floor)

W

up <sup>20.4</sup> 16.5 <sup>25.0</sup> 15.9 <sup>31.5</sup> 9.4 2.6  
300 200 100

Ref spk Loc SW of X  
Sly S.H. Mon Not #322 (ref. point)

5.8  
20.0 14.7 14.4 19.7  
FL Hdwl 7.7 Hdwl FL

T.P. 5.63 1240.90 6.92 1235.27

96 31.9✓

95 38.9✓

T.P. 0.0 1242.19 12.14 1242.19

94 8.4 45.9✓

T.P. 0.0 1254.33 12.94 1254.33

93 12.4 54.9✓

92 5.0 62.3✓

T.P. 0.0 1267.27 12.89 1267.27

91 12.1 68.1✓

90 72.0✓

89 73.9✓

88+50 75.4✓

88 75.6✓

87 75.7✓

86 76.5✓

85 77.8✓

84 78.8✓

T.P. 1.41 1280.16 3.96 1278.75

83 76.8✓

82 74.5✓

81+29 74.4✓

1282.71

W E E 61

30 24 15 Gd.rail 7.7 7.3 GR. 14 24 30  
11.5 11.7 8.4 12 11 13 7.4 12.5 12.8

57795  
3.3

BM 7.16  
No 6.9  
chd 7.1  
7.0 0.6  
✓ 6.4 1.6  
4.8 2.4  
2.4

$\frac{30}{8.4}$   $\frac{16}{8.8}$   $\frac{10}{8.8}$  8.2

$\frac{9}{8.4}$   $\frac{16}{9.0}$   $\frac{30}{9.1}$

63

48

46

45

37

24

$\frac{30}{1.7}$   $\frac{13}{1.4}$   $\frac{12}{2.1}$  1.4  $\frac{13}{1.9}$  +0.5 18 +1.2 30

5.9

8.2

15.6 12.2 8.4 8.3

100' FL Hdwl

8.4 12.0  
Hdwl FL

B.M. 8.40 1274.31

~~81~~ 80 81=8.3 74.4 ✓

~~80~~ 79 76.8 ✓

T.P. 6.05 1282.71 12.84 1276.66

~~79~~ 78 79.1 ✓

~~78~~ 77 83.5 ✓

T.P. 0.79 1289.51 11.79 1288.71

~~77~~ 76 9.9 90.6 ✓

~~76~~ 75 2.7 1297.8 ✓

T.P. 0.0 1300.51 12.49 1300.51

~~75~~ 74 13 03.6 ✓

~~74~~ 73 07.9 ✓

~~73~~ 72 10.2 ✓

~~72~~ 71 11.7 ✓

B.M. 0.78 1312.21

70 70 0.5 ✓ 12.5 ✓

T.P. 0.56 1312.99 11.59 1312.43

69 14.1 ✓

68 16.6 ✓

67 19.8 ✓

66 21.5 ✓

1324.02

W

E

62

NW & West culvert hdwl

8.3 ✓

5.9 ✓

10.4 ✓

$\frac{30}{3.8} \frac{20}{4.2} \frac{13}{7.0} \frac{9}{6.4}$

6.0

$\frac{12.5}{7.0} \frac{15}{8.1} \frac{23}{3.8} \frac{30}{2.8}$

2.4

9.4

5.1

2.8

$\frac{30}{1.9} \frac{16}{1.5} \frac{13}{2.4} \frac{10.5}{1.4}$

1.3

$\frac{12.5}{1.5} \frac{16}{0.6} \frac{30}{-1}$

Ref spk SE side 30" Map front of N end Varney's house

4.6

0.9

3.8

FL

± FL

9.9

7.4

4.2

4.4 4.3 3.2

2.5

2.5

2.9

1.9

1.2

30

20

9.5

7.5

8.5

18.5

30

13

65 23.9 ✓

T.P. 1.01 1324.02 9.23 1323.01

64 26.2 ✓

63 28.5 ✓

62 point 2-18 31.7 ✓

T.P. 0.78 1332.24 9.31 1331.46

61 35.1 ✓

60 36.3 ✓

59 36.7 ✓

58 37.5 ✓

57 38.0 ✓

T.P. 1.25 1340.77 2.18 1339.52

BM#5 0.11 1341.59 1341.7

56 36.8

55 34.8

54 +0.04 33.1

TP#X 10.14 1341.70 1331.52

T.P. 6.95 1338.47

for Bear Rd

W

63

0.1

6.0

3.7

0.5

stk 6' back of ditch 62+25

5.7

30 17 12 9 7 11 14.5 24 30  
6.1 5.9 5.3 4.9 4.5 4.8 5.3 7.4 1.6

4.1

3.3

2.8

Spk SW side 18" Ash 1st N Cushing Dr

4.9

6.9

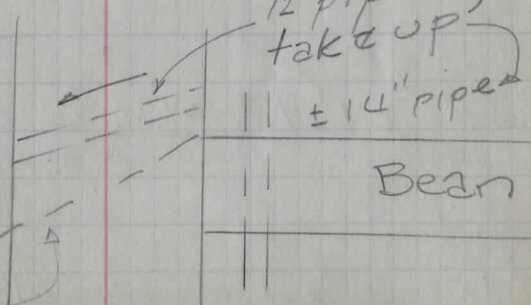
30 20 13 7 8.6 5 9 12 13 19 30  
10.2 9.4 9.6 9.1 8.6 8.8 9.0 9.7 9.7 7.4 5.0

12" pipes take up

± 14" pipe

Bear

put in need 15" pipe



1338.47  
 53 Bean Rd

T.P. 12.18 1349.95 0.70 1337.77

53 Bean Rd  
 T.P. 12.9 1362.85 0.0 1349.95

53 Bean

T.P. <sup>4</sup>X 10.12 2.11 1331.52

52 25.1

51 23.2

T.P. 11.22 1333.63 7.45 1322.41

50 22.6

49+99

49 23.4

48 25.7

47 26.3

46+81 26.6

46 28.4

T.P. 1.24 1329.86 10.64 1328.62

45 33.6

44 38.7

T.P. <sup>7 3/4</sup> 0.65 1339.26 5.31 1338.61

30.0 33.7 37.8  
 8.5 4.8 .70  
 30 100

46.9  
 3.1  
 200

56.6  
 6.2  
 300

62.4  
 0.4 summit  
 380 ± 500

F.L. TOP  
 10.7 7.3 7.3

TOP  
 7.2 F.L. 10.3

30 18 13.5 8.5  
 3.6 3.5 5.2 4.5 4.2  
 F.L. 3.6  
 8.2 3.3  
 1.5

6.5  
 6 12 14 20 30  
 4.5 49.5.3 21.5 1.8  
 F.L. 6.1

5.7  
 0.6

	+	HI	-	E
BM #4	5.46	1343.92		1338.46
BM #1	6.04	1344.58	✓	1338.54
T.P.	1.23	1339.90	✓ 5.91	1338.67 ✓
T.P.	1.22	1329.92	✓ 11.20	1328.70 ✓
T.P.	11.19	1333.69	7.42	1322.50 (1322.49)
T.P.			2.05	1331.64 (1331.60)
BM	7.99	1245.01		1237.02
Sta 99				38.8
100' E				45.0
Sta 100				45.0
T.P. E			0.02	1244.99
T.P. N	4.81	1249.79	0.03	1244.98
Sta 101				48.1
" 102				44.8
" 103				40.0
T.P. E	13.23	1258.22		1244.99
200' E				51.1
300' E				56.3
340' E				58.2

To find 1.0' Error

Loc SW 1/4 intersect #4E 322

6.2

0.02

0.03

1.7

5.0

9.8

7.1

1.9

0.0

3-18-48

## SOUNDINGS

W

E

27 to	0" / 7'	1" / 6'	12"	1" / 9'
-------	---------	---------	-----	---------

12 to	2" / 9'	9"	2" / 6'	1" / 9'
-------	---------	----	---------	---------

24 to	0" / 9'	2 1/2" / 3'	2"	2" / 3'	0" / 9'
-------	---------	-------------	----	---------	---------

Road good cond

33 to	3" / 6'	8"	sand & clay	9'
-------	---------	----	-------------	----

Not much stone & very small

34 to	3" / 8'	14"	2" / 8'	Sandy soil
-------	---------	-----	---------	------------

Sandy soil

54	2" / 10'	2" / 5'	2" / 6'	2" / 6'
----	----------	---------	---------	---------

top crown

E

66

63 to	3" / 9'	4"	1" / 7'
-------	---------	----	---------

76 to	1" / 8'	12"	2" / 8'
-------	---------	-----	---------

86 to	3" / 9'	3"	4" / 9'
-------	---------	----	---------

95	12" / 9'	14" / silica & slag	12" / 8'
----	----------	---------------------	----------

1/21/50 Pam Maynard Post

AUBURN ROAD

B.M. 11.6 1323.03 1311.43  
 0+0 7.9 15.1

#8 West

22.7  
 0.3  
 600

#4 South

B.M. 1.48 1312.91 1311.43

#8 North east

T.P. 0.10 1300.09 12.92 1299.99

#8 north East

No 4 north

B.M. 0.92 1312.35 1311.43

1+0 0.0 12.3

2+0 3.0 09.3

3+0 7.1 05.7

4+0 11.7 00.6

T.P. 0.21 1300.24 12.32 1300.03

5+0 3.7 96.5

6+0 7.3 92.9

7+0 10.5 89.7

8+0 13.1 87.1

C.H. #4 PQR

Spk SW root 36" Maple 100' Rt Sta  
 1+0

22.5 22.2 21.9 20.4 18.0 15.1  
 0.5 0.8 1.1 2.6 5.0 7.9  
 500 400 300 200 100

23.3 22.1 20.3 18.7 16.7 15.1  
 ± - 0.2 0.9 2.7 4.3 6.1 7.9  
 500 400 300 200 100

04.8 10.2  
 8.1 2.7  
 300 200 100

83.2 90.4 98.0  
 16.9 9.7 2.1  
 500 400 300

T.P.	1.10	1288.70	12.64	1287.60
------	------	---------	-------	---------

8+82 culvt

9+0			3.5	85.2
B.M.			3.28	1285.42 (1285.44)

10+0 4.7 84.0

11+0 6.3 82.4

12+0 7.8 80.9

13+0 8.8 79.9

T.P.	0.26	1280.50	8.46	1280.24
------	------	---------	------	---------

14+0 1.7 78.8

15+0 3.3 77.7

16+0 5.5 75.0

17+0 8.1 72.4

18+0 9.7 70.8

19+0 10.5 70.0

T.P.	6.44	1276.22	10.72	1269.78
------	------	---------	-------	---------

20+0

20+17 culvt

21+0 5.9 70.3

22+0 4.5 71.7

23+0 4.6 71.6

24+0 4.8 71.4

25+0 5.9 70.3

26+0 7.2 69.0

85.6

5.0	31	5.7	7.7
FL		FL	± 80'

8.4	9.4	7.4	6.7	7.0	8.9	5.5	4.9
30	17	13		11	15	21	30

69.5

10.0	6.7	9.1
FL		FL

27+0			8.5	67.7
T.P.	1.98	1270.08	8.12	1268.10
28+0			3.8	66.3
+76	colut			
29+0			4.9	65.2
30+0			5.1	65.0
B.M. #4			1.57	1268.51 (68.47)
31+0			4.8	65.3
32+0			6.7	63.4
33+0			8.8	61.3
+99	colut			
T.P.	12.92	1273.93	9.07	1261.01
35+0	6.92	1267.93	7.9	60.0
36+0			7.4	60.5
37+0			6.0	61.9
38+0			2.7	65.2
+50			2.0	65.9
39+0			2.1	65.8
40+0			5.0	62.9
+24	colut			
41			6.1	61.8
42			3.1	64.8
T.P.	7.61	1278.76	2.78	1271.15
43		1272.76	4.5	65.15 -68.3
44			3.0	69.8

65.4  
8.0 4.7 7.6  
FL FL

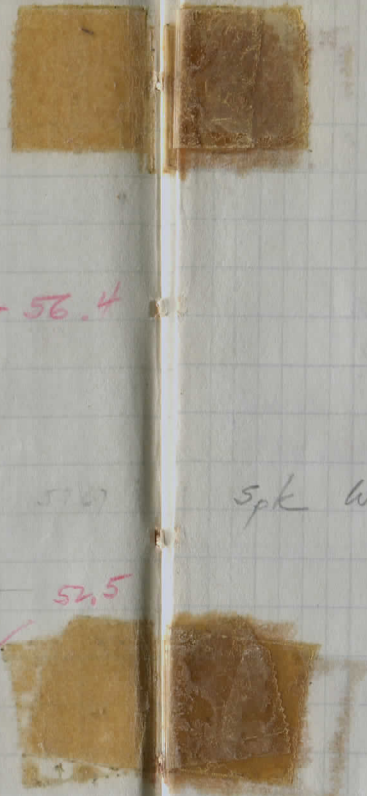
13.1 59.6 12.4  
6.4 3.6  
19.5 10.5 16.0  
FL FL

B.M. set W. root Maple + 30' int 39+90  
Elev = 1262.80

11.4 10.9 6.7 5.8 5.0 5.5 7.0 7.6  
30 21 15 10 10 18 30  
62.3  
13.0 5.6 10.7  
FL FL

~~1278.76~~  
72.76 ✓

45 3.5 69.3  
 46 6.2 66.6  
 47 10.9 61.9  
 T.P. 0.08 1266.47 12.37 ~~1266.39~~  
 48 1260.47 ✓ 41 ~~60.39~~ 56.4  
 49 7.4 53.1  
 + 48 col/ut  
 50 6.9 53.6  
 B.M. <sup>set</sup> 2.51 1257.96  
 51 7.8 52.7  
 T.P. 2.38 ~~1261.70~~ 7.15 ~~1257.32~~ 52.5  
 52 1255.70 3.2 ~~1253.32~~  
 53 3.7 52.0  
 54 4.4 51.3  
 + 68 col/ut  
 55 4.8 ✓ 50.9  
 56 3.7 ✓ 52.0  
 57 2.8 52.9  
 58 2.2 53.5  
 T.P. 10.96 ~~1270.90~~ 1.76 ~~1259.94~~ in red  
 58+13 = intersect 11.3 53.94 53.6  
 B.M. 9.10 ~~1255.80~~ (55.87)  
 Thuring Red E  
 T.P. 12.32 1277.00 0.22 64.68



53.1  
 15.6 7.4 13.9  
 F.L. FL

Spk W root 36" W.C.K. ntg 50+20

9.3 5.0 7.7  
 FL FL

Spk E root 16" maple 30' Rt + 57+85

57.6 62.3  
 7.3 2.6  
 100 200

67.8 73.5 77.0  
 9.2 3.5 0.0  
 300 400 462

T.P. 0.25 54.19 0.25 1253.94  
 showing Rf west

41.7 43.4

45.1 47.2 49.3

10.8 9.1 7.0 4.9  
 500 400 300 200 100

chk  
 BM 3.25 1267.21 1263.98  
 T.P. 12.30 1278.69 0.82 1266.39  
 T.P. 2.28 1276.28 4.69 1274.00 correct  
 BM set 7.48 1268.80 1262.80  
 T.P. 9.26 1267.02

Wd Cherry

W root, <sup>hand</sup> maple to rd of 39+90

67.21  
 .82  
 ---  
 66.39

B.M. 4.05 1259.85 9.05 1255.80 1256.17

54.5

59+0

5.3

55.7

60+0

$\frac{5.6}{30}$	$\frac{5.1}{17}$	$\frac{6.3}{13+14}$	$\frac{5.2}{11}$	4.1	$\frac{4.8}{13}$	$\frac{5.5}{16}$	$\frac{1.9}{22}$	$\frac{1.3}{30}$
------------------	------------------	---------------------	------------------	-----	------------------	------------------	------------------	------------------

61+0

56.2

3.6

62+0

56.1

3.7

63+0

55.6

4.2

T.P. 7.37 1262.56 4.66 1255.19

56.4

64+16

COBY

$\frac{10.4}{E100}$	$\frac{9.4}{WFL}$	6.2	$\frac{8.4}{EFL}$
---------------------	-------------------	-----	-------------------

65+0

57.1

5.5

66+0

57.9

4.7

67+0

57.7

4.9

69+0

56.2

6.4

70+34

55.1

$\frac{12.2}{100.}$	$\frac{11.0}{WFL.}$	7.5	$\frac{10.2}{EFL.}$
---------------------	---------------------	-----	---------------------

1262.56 ✓

1255.19

73

77. 3.15 1257.93 7.78 1254.78

71+0

72+0

73+0

74+50

75+0

75+19

76+30

77+0

79+0

T.P. 5.09 1262.27 0.75 1257.18

B.M. 2.82 1259.45 (59.42)

80+0

81+0

82+0

W

E

54.8

3.1

55.3

2.6

54.6

3.3

52.9

5.0

53.4

4.5

53.6

8.9  
#1008.5  
W.F.L.

4.3

8.4

E.F.L.

52.8

5.1

53.1

4.8

57.4

0.5

Spk W root 24" maple

30' Rt 79+40

58.1

3.9	5.3	4.8	6.0	5.1	4.2	4.7	5.3	4.1
30	30	19	16	13		13	16	19

58.2

4.1

57.5

4.8

1262.27 ✓

1257.18

W

E

74

82+54

CULV

 $\frac{9.1}{2100}$ 7.4  
WFL

57.4

4.9

 $\frac{6.9}{EFL}$ 

84+0

58.0  
4.3

86+0

56.3  
5.9

T.P

7.99 1263.66 6.60 1255.67

85+19 Build ± 15" X road cut

Skew NW (Creek comes in from <sup>due E</sup>)

86+40 to 87+0 WASHOUT

87+13

RE-LAY

CULV

 $\frac{10.46}{290}$  $\frac{10.18}{200}$ 

10.1

10.1

7.4

53.56 56.3

± 100 SW of  
STONE CULV

200

100 NWLY

WFL

88+0

56.9  
6.8

89+24

CULV

58.9

8.42

9.8

9.02

WFL

EFL

90+0

59.0  
4.7

92+0

61.5  
2.2

T.P

13.28 1275.94 1.0 1262.66

93+30

66.97  
9.0

94+0

73 - 68.6

95+0

69.5  
6.4

96+0

71.5  
4.4

1275.94

1262.66

96+61

± E U.S.R.76

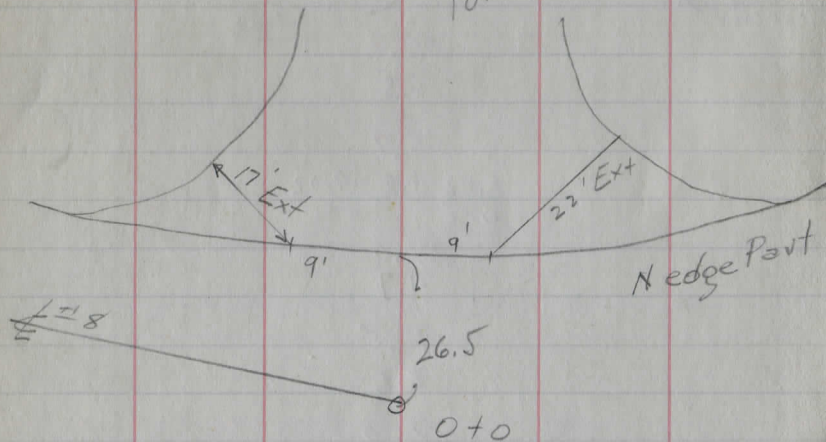
B.M. X SEP HOWELL STAFF

GOVE JULY 1950

2.02 1273.92 (73.82)

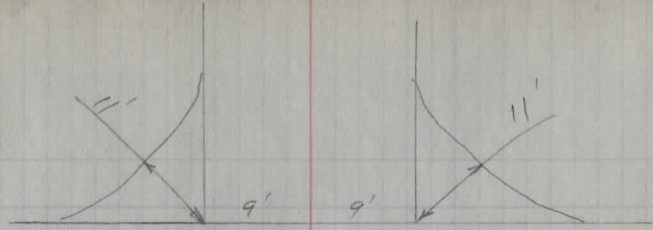
Cont'd BK # 168

TURN OUTS #4 & #8

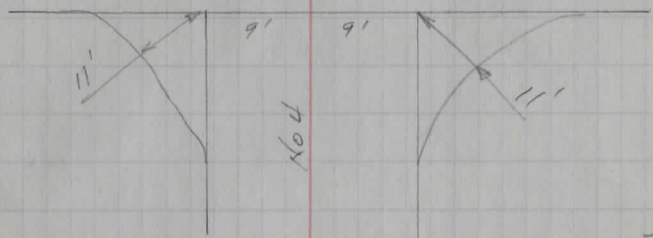


7/11

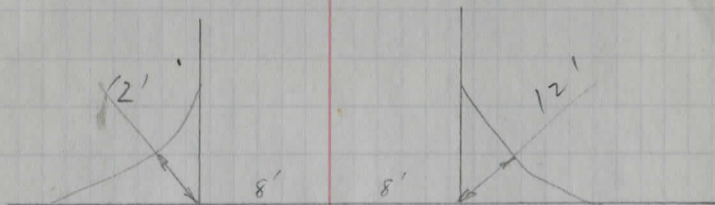
N  
↑



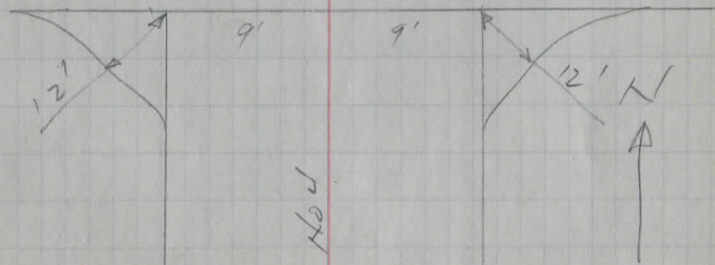
# 27 part



see pg 77



E & G part





25'  
25'  
30'  
30'

.60 <sup>c</sup> 140 ± 42

.60-.615  $\epsilon$  busted  $\epsilon$  edge Ute on  $\epsilon$   
 32  $\pm 3'$  east  
 31 patches broken  $\pm 60'$  each  
 .30 way from summit of hill

.22-26 patched & patches broken.  
 .25  
 .23  
 .22

Highest bank is on  $\epsilon$ . How about draw near  $\epsilon$  edge of part II to  $\epsilon$  over top of hill

.21  
 .20 - 26 busted up on  $\epsilon$

.20  
 40.18 20' bust up on  $\epsilon$

.92 Big bust up last spring. Is hard now  
 .86 dry good ditches

39.825  
 39.82  
 39.80  
 39.77

Route #6 ← Speedometer

neck drive

41.02

bust on  $\epsilon$  not drainage val 77

160 ± 30 end bad bust

FRENCH DRAINS  
 Found July 1951  
 Aub. Rd #4 PQR

.98 = 159 ± 75  
 $\pm$  summit  
 .945  
 .93 <sup>c</sup> 157 ± 85

.88 = 154 ± 90

Bad bust north on  $\epsilon$  here over top of hill high bank on  $\epsilon$

.85 = 40' bust not bad

.80 = 151 ± 0 20' bust on  $\epsilon$  (not bad)

147 ± 30 - 148 ± 30

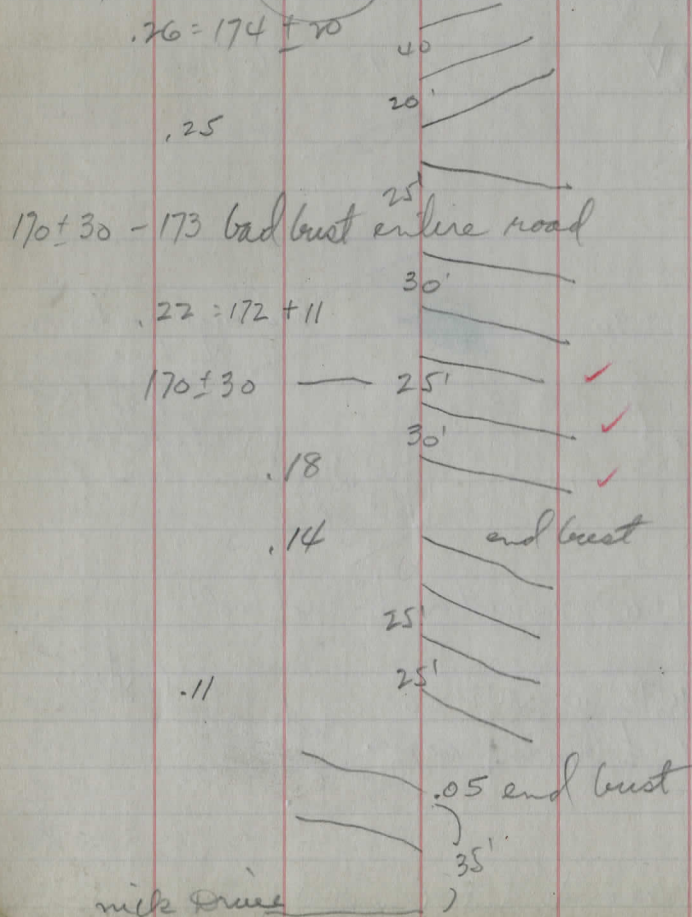
.72-.74  $\epsilon$  breaking some not to bad extra

.70  
 .67  
 .65  $\pm$  20' on  $\epsilon$  starting to bust

B.M.'s Downings Corners, North Rd.

B.M. #1	1313.24
" #2	1285.51
" 3	1267.90
" 4	1268.59
" 5	1262.55
" 6	1257.73
" 7	1253.87

7  
182 ± 99



Spk. W. Root 30" Map	100' Rt #0+30,
" E " 15" "	25' Lt # 9+90
" " " " "	" " " 20+15
" W " 24" "	" Rt " 30+10
" " " 30" "	30' " " 39+90
" " " 24" W.Ch	25' " " 50+20
" E " 10" Map	30' " E 57+95

1st

inlet	8.3	-0.0
	8.3	-2.4
	5.9	-23
	3.6	

2nd

	7.1	-0.1
	7.0	-0.6
	6.4	-1.6
	4.8	-2.4

9' E of E ± 1+50

8' W of E ± 10+00

6' E of E ± 20+00

± 30+00

6' W of E ± 40+00

9' E of E ± 50+00

8' E of E ± 60+00 2<sup>nd</sup> PL of Tramp

26 00

16 96.7

903.3 / .11000

9033

19670

9' W of E ± 70+00

± 80+00

9' E of E ± 90+00

39' W of Stake 100+00

25' W of Stake 110+00

± 120+00

7' W of E 130+00

30' W of Stake 140+00

24' W of Stake 150+00

57' W of Stake 162+00

170+00

30' E of Stake 180+00

35' E of Stake at Reservoirs

6" Gravel 9' W of E Travel

10" Gravel & Travel

5" Gravel 8' W of E Drain

5" Gravel 3 1/2' E of Stake

8" Gravel E Edge Travel

5" Gravel & Travel

9" Gravel 5' E of Stake

6" Gravel & Travel

9" Gravel 3' E. E Travel

7" Gravel 3' W of W Travel

5" Gravel & Travel

4" Gravel 5' W of E Edge 32

5" gravel

4"

5"

10" Gravel 9' W of Stake

6" Gravel 9' W of Stake

10" Gravel

9" Gravel m & Travel

5" Sand E Travel N Traffic

2" W 6' W of E Stake

20' W of Stake  
10' E of W Stake

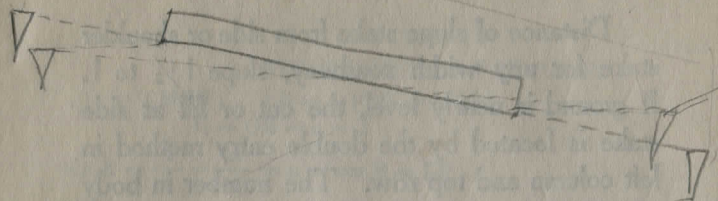
9' W of Stake  
& Travel

6' W of Stake

E Travel N Traffic

6' W of E Stake

53  
27  
19



## IMPROVED TABLES

AND

## INFORMATION

9/4 4298  
92+24  
43560  
217800  
2094  
840  
698  
1420

11.8  
8.2  
20.0

400 inter pipe  
294 from back # to inter

12.8  
4.1  
376  
350  
26

376-26

48.73  
ref. to 9.L.

62.75  
25  
37.75

244200  
217800  
264000

8  
43560

312  
34800  
2094  
244200

698  
350

PLEASE RETURN TO  
GEAUGA COUNTY ENGINEER

COURT HOUSE  
CHARDON, O.  
PHONE 250-X

TABLE OF INCHES REDUCED TO DECIMALS OF A FOOT.

Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.
1	.0052	1	.1094	2	.2135	3	.3177	4	.4219	5	.5260
1	.0104	1	.1146	2	.2188	3	.3229	4	.4271	5	.5313
1	.0156	1	.1198	2	.2240	3	.3281	4	.4323	5	.5365
1	.0208	1	.1250	2	.2292	3	.3333	4	.4375	5	.5417
1	.0260	1	.1302	2	.2344	3	.3385	4	.4427	5	.5469
1	.0312	1	.1354	2	.2396	3	.3438	4	.4479	5	.5521
1	.0364	1	.1406	2	.2448	3	.3490	4	.4531	5	.5573
1	.0416	1	.1458	2	.2500	3	.3542	4	.4583	5	.5625
1	.0468	1	.1510	2	.2552	3	.3594	4	.4635	5	.5677
1	.0520	1	.1562	2	.2604	3	.3646	4	.4688	5	.5729
1	.0572	1	.1614	2	.2656	3	.3698	4	.4740	5	.5781
1	.0624	1	.1666	2	.2708	3	.3750	4	.4792	5	.5833
1	.0676	1	.1718	2	.2760	3	.3803	4	.4844	5	.5885
1	.0728	1	.1770	2	.2813	3	.3854	4	.4896	5	.5938
1	.0780	1	.1822	2	.2865	3	.3906	4	.4948	5	.5990
1	.0832	1	.1874	2	.2917	3	.3958	4	.5000	5	.6042
1	.0884	1	.1926	2	.2969	3	.4010	4	.5052	5	.6094
1	.0936	1	.1978	2	.3021	3	.4063	4	.5104	5	.6146
1	.0988	1	.2030	2	.3073	3	.4115	4	.5156	5	.6198
1	.1040	1	.2082	2	.3125	3	.4167	4	.5208	5	.6250
1	.1092	1	.2134	2	.3177	3	.4219	4	.5260	5	.6302
1	.1144	1	.2186	2	.3229	3	.4271	4	.5313	5	.6354
1	.1196	1	.2238	2	.3281	3	.4323	4	.5365	5	.6406
1	.1248	1	.2290	2	.3333	3	.4375	4	.5417	5	.6458
1	.1300	1	.2342	2	.3385	3	.4427	4	.5469	5	.6510
1	.1352	1	.2394	2	.3438	3	.4479	4	.5521	5	.6563
1	.1404	1	.2446	2	.3490	3	.4531	4	.5573	5	.6615
1	.1456	1	.2498	2	.3542	3	.4583	4	.5625	5	.6667
1	.1508	1	.2550	2	.3594	3	.4635	4	.5677	5	.6719
1	.1560	1	.2602	2	.3646	3	.4688	4	.5729	5	.6771
1	.1612	1	.2654	2	.3698	3	.4740	4	.5781	5	.6823
1	.1664	1	.2706	2	.3750	3	.4792	4	.5833	5	.6875
1	.1716	1	.2758	2	.3803	3	.4844	4	.5885	5	.6927
1	.1768	1	.2813	2	.3854	3	.4896	4	.5938	5	.6979
1	.1820	1	.2865	2	.3906	3	.4948	4	.5990	5	.7031
1	.1872	1	.2917	2	.3958	3	.5000	4	.6042	5	.7083
1	.1924	1	.2969	2	.4010	3	.5052	4	.6094	5	.7135
1	.1976	1	.3021	2	.4063	3	.5104	4	.6146	5	.7188
1	.2028	1	.3073	2	.4115	3	.5156	4	.6198	5	.7240
1	.2080	1	.3125	2	.4167	3	.5208	4	.6250	5	.7292
1	.2132	1	.3177	2	.4219	3	.5260	4	.6302	5	.7344
1	.2184	1	.3229	2	.4271	3	.5313	4	.6354	5	.7396
1	.2236	1	.3281	2	.4323	3	.5365	4	.6406	5	.7448
1	.2288	1	.3333	2	.4375	3	.5417	4	.6458	5	.7500
1	.2340	1	.3385	2	.4427	3	.5469	4	.6510	5	.7552
1	.2392	1	.3438	2	.4479	3	.5521	4	.6563	5	.7604
1	.2444	1	.3490	2	.4531	3	.5573	4	.6615	5	.7656
1	.2496	1	.3542	2	.4583	3	.5625	4	.6667	5	.7708
1	.2548	1	.3594	2	.4635	3	.5677	4	.6719	5	.7760
1	.2600	1	.3646	2	.4688	3	.5729	4	.6771	5	.7813
1	.2652	1	.3698	2	.4740	3	.5781	4	.6823	5	.7865
1	.2704	1	.3750	2	.4792	3	.5833	4	.6875	5	.7917
1	.2756	1	.3803	2	.4844	3	.5885	4	.6927	5	.7969
1	.2808	1	.3854	2	.4896	3	.5938	4	.6979	5	.8021
1	.2860	1	.3906	2	.4948	3	.5990	4	.7031	5	.8073
1	.2912	1	.3958	2	.5000	3	.6042	4	.7083	5	.8125
1	.2964	1	.4010	2	.5052	3	.6094	4	.7135	5	.8177
1	.3016	1	.4063	2	.5104	3	.6146	4	.7188	5	.8229
1	.3068	1	.4115	2	.5156	3	.6198	4	.7240	5	.8281
1	.3120	1	.4167	2	.5208	3	.6250	4	.7292	5	.8333
1	.3172	1	.4219	2	.5260	3	.6302	4	.7344	5	.8385
1	.3224	1	.4271	2	.5313	3	.6354	4	.7396	5	.8438
1	.3276	1	.4323	2	.5365	3	.6406	4	.7448	5	.8490
1	.3328	1	.4375	2	.5417	3	.6458	4	.7500	5	.8542
1	.3380	1	.4427	2	.5469	3	.6510	4	.7552	5	.8594
1	.3432	1	.4479	2	.5521	3	.6563	4	.7604	5	.8646
1	.3484	1	.4531	2	.5573	3	.6615	4	.7656	5	.8698
1	.3536	1	.4583	2	.5625	3	.6667	4	.7708	5	.8750
1	.3588	1	.4635	2	.5677	3	.6719	4	.7760	5	.8802
1	.3640	1	.4688	2	.5729	3	.6771	4	.7813	5	.8854
1	.3692	1	.4740	2	.5781	3	.6823	4	.7865	5	.8906
1	.3744	1	.4792	2	.5833	3	.6875	4	.7917	5	.8958
1	.3796	1	.4844	2	.5885	3	.6927	4	.7969	5	.9010
1	.3848	1	.4896	2	.5938	3	.6979	4	.8021	5	.9063
1	.3900	1	.4948	2	.5990	3	.7031	4	.8073	5	.9115
1	.3952	1	.5000	2	.6042	3	.7083	4	.8125	5	.9167
1	.4004	1	.5052	2	.6094	3	.7135	4	.8177	5	.9219
1	.4056	1	.5104	2	.6146	3	.7188	4	.8229	5	.9271
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1	.4316	1	.5365	2	.6406	3	.7448	4	.7500	5	.9531
1	.4368	1	.5417	2	.6458	3	.7500	4	.7552	5	.9583
1	.4420	1	.5469	2	.6510	3	.7552	4	.7604	5	.9635
1	.4472	1	.5521	2	.6563	3	.7604	4	.7656	5	.9688
1	.4524	1	.5573	2	.6615	3	.7656	4	.7708	5	.9740
1	.4576	1	.5625	2	.6667	3	.7708	4	.7760	5	.9792
1	.4628	1	.5677	2	.6719	3	.7760	4	.7813	5	.9844
1	.4680	1	.5729	2	.6771	3	.7813	4	.7865	5	.9896
1	.4732	1	.5781	2	.6823	3	.7865	4	.7917	5	.9948
1	.4784	1	.5833	2	.6875	3	.7917	4	.7969		
1	.4836	1	.5885	2	.6927	3	.7969	4	.8021		
1	.4888	1	.5938	2	.6979	3	.8021	4	.8073		
1	.4940	1	.5990	2	.7031	3	.8073	4	.8125		
1	.4992	1	.6042	2	.7083	3	.8125	4	.8177		
1	.5044	1	.6094	2	.7135	3	.8177	4	.8229		
1	.5096	1	.6146	2	.7188	3	.8229	4	.8281		
1	.5148	1	.6198	2	.7240	3	.8281	4	.8333		
1	.5200	1	.6250	2	.7292	3	.8333	4	.8385		
1	.5252	1	.6302	2	.7344	3	.8385	4	.8438		
1	.5304	1	.6354	2	.7396	3	.8438	4	.8490		
1	.5356	1	.6406	2	.7448	3	.8490	4	.8542		
1	.5408	1	.6458	2	.7500	3	.8542	4	.8594		
1	.5460	1	.6510	2	.7552	3	.8594	4	.8646		
1	.5512	1	.6563	2	.7604	3	.8646	4	.8698		
1	.5564	1	.6615	2	.7656	3	.8698	4	.8750		
1	.5616	1	.6667	2	.7708	3	.8750	4	.8802		
1	.5668	1	.6719	2	.7760	3	.8802	4	.8854		
1	.5720	1	.6771	2	.7813	3	.8854	4	.8906		
1	.5772	1	.6823	2	.7865	3	.8906	4	.8958		
1	.5824	1	.6875	2	.7917	3	.8958	4	.9010		
1	.5876	1	.6927	2	.7969	3	.9010	4	.9063		
1	.5928	1	.6979	2	.8021	3	.9063	4	.9115		
1	.5980	1	.7031	2	.8073	3	.9115	4	.9167		
1	.6032	1	.7083	2	.8125	3	.9167	4	.9219		
1	.6084	1	.7135	2	.8177	3	.9219	4	.9271		
1	.6136	1	.7188	2	.8229	3	.9271	4	.9323		
1	.6188	1	.7240	2	.8281	3	.9323	4	.9375		
1	.6240	1	.7292	2	.8333	3	.9375	4	.9427		
1	.6292	1	.7344	2	.8385	3	.9427	4	.9479		
1	.6344	1	.7396	2	.8438	3	.9479	4	.9531		
1	.6396	1	.7448	2	.8490	3	.9531	4	.9583		
1	.6448	1	.								

FB 158  
PS 182

AUBURN ROAD

ART TEMPLES NOTES  
1992

58+08.94

Boat Spk  
fd 51

Bartholomew

O.C.E.I  
581276

sw  
10" Walnut

42+18.04  
POT

ok  
31.0

Fd out 92

1.P. set 33.0

1268  
3368  
900

sw  
S.W. side  
18" MAP  
2' up

ok  
66.12

sw  
N. side  
12 map

38.21

bolt set 51  
I.P. fd. 0.78 SW of above

33+18.40  
Δ = 00-20' RT

Fd out 92

31.08  
Point  
Point  
SLOPE

ok Vert Spk  
SW root  
50" MAP.

33+18  
21 87  
11 61

Good oct 92

Good oct 92

sw  
SW side  
cherry

46.25

85.68

Fd oct 92

1/2" I. Pin set 51

21+87  
Δ = 00-10' LT

Good oct 92

Pole  
97PI

77.90

good oct 92

Pole  
97PI

55.24

0+0

Portage Co

Fd oct 92

I.P. fd 73  
fd 89

COUNTY LINE

